

Notes

- ◆ Please read
 - O'Brien and Hodgins, "Graphical modeling and animation of brittle fracture", SIGGRAPH '99
 - O'Brien, Bargteil and Hodgins, "Graphical modeling and animation of ductile fracture", SIGGRAPH '02, pp. 291--294.

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Discrete Mean Curvature

- ◆ [draw triangle pair]
 - ∪ κ for that chunk varies as $\kappa \sim \frac{\theta}{h_1 + h_2}$
 - ◆ So integral of κ^2 varies as $W = \sum_e \frac{\theta^2}{(h_1 + h_2)^2} (|\Delta_1| + |\Delta_2|)$
 $\sim \sum_e \frac{\theta^2 |e|^2}{|\Delta_1| + |\Delta_2|}$
- ◆ Edge length, triangle areas, normals are all easy to calculate
 - ∪ θ needs inverse trig functions
 - ∪ But θ^2 behaves a lot like $1 - \cos(\theta/2)$ over interval $[-\pi, \pi]$ [draw picture]

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Bending Force

- ◆ Force on x_i due to bending element involving i is then

$$F_i = -B \frac{\partial W}{\partial x_i} \sim -B \frac{|e|^2}{|\Delta_1| + |\Delta_2|} \sin\left(\frac{\theta}{2}\right) \frac{\partial \theta}{\partial x_i}$$

- ◆ Treat first terms as a constant (precompute in the rest configuration)

$$\sin \frac{\theta}{2} = \pm \sqrt{\frac{1}{2}(1 - n_1 \cdot n_2)}$$

- ◆ Sign should be the same as $\sin \theta = n_1 \times n_2 \cdot \hat{e}$
- ◆ Still need to compute $\partial \theta / \partial x_i$

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Gradient of Theta

- ◆ Can use implicit differentiation on $\cos(\theta) = n_1 \cdot n_2$
 - Not too much fun
 - Automatic differentiation: Grinspun et al. "Discrete Shells, SCAN'03
 - Modal analysis: Bridson et al., "Simulation of clothing...", SCA'03

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Damping hyper-elasticity

- ◆ Suppose W is of the form $C \cdot C / 2$
 - C is a vector or function that is zero at undeformed state
- ◆ Then $F = -\partial C / \partial X \cdot C$
 - C says how much force, $\partial C / \partial X$ gives the direction
- ◆ Damping should be in the same direction, and proportional to $\partial C / \partial t$:
 $F = -\partial C / \partial X \cdot \partial C / \partial t$
- ◆ Can simplify with chain rule:
 $F = -\partial C / \partial X \cdot (\partial C / \partial X v)$
 - Linear in v , but not in $x \dots$

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Hacking in strain limits

- ◆ Especially useful for cloth:
 - Biphasic nature: won't easily extend past a certain point
- ◆ Sweep through elements (e.g. springs)
 - If strain is beyond given limit, apply force to return it to closest limit
 - Also damp out strain rate to zero
- ◆ No stability limit for fairly stiff behaviour
- ◆ See X. Provot, "Deformation constraints in a mass-spring model to describe rigid cloth behavior", Graphics Interface '95

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Elastic Collisions

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Simplest approach

- ◆ Treat it just as a particle system:
 - Check if (surface) particles hit objects
 - Process collisions independently if so
- ◆ Inelastic collisions (and simplified resolution algorithm) are perfectly appropriate
 - Elasticity/damping inside object itself provides the rebound...
- ◆ Problems:
 - Coupling with uncollided particles?
 - Thin objects (like cloth or hair)?
 - Deformable vs. deformable?

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Coupling with rest of object

- ◆ Velocity smoothing:
 - Figure out collision velocity, call it $v_{n+1/2}$
 $x_{n+1} = x_n + \Delta t v_{n+1/2}$
 - Then do an implicit velocity update:
 $v_{n+1} = v_{n+1/2} + \Delta t/2 a(x_{n+1}, v_{n+1})$
 - See Bridson et al., "Robust treatment of collisions...", SIGGRAPH '02
- ◆ Stronger velocity smoothing
 - Constrain normal velocity of colliding nodes
 - See Irving et al., "Invertible finite elements...", SCA '04
- ◆ Couple into full implicit solve (position as well)
 - See Baraff & Witkin, "Large steps in cloth simulation", SIGGRAPH '98

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Thin objects

- ◆ Collision detection is essential
 - Otherwise particles will jump through objects
- ◆ But not enough
 - Triangle mesh vs. mesh requires point vs. face AND edge vs. edge
 - Otherwise we can have significant tangling

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Distributing impulses

- ◆ If an edge collides, how do we distribute impulse between two endpoints?
- ◆ If a triangle collides, how do we distribute impulse between three corners?
- ◆ Weight with barycentric coordinates
 - And require that interpolated point change in velocity is what is required
- ◆ See Bridson et al., "Robust treatment...", SIGGRAPH '02

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Scalable collision processing

- ◆ Cloth: fixing one collision can cause others
 - Easy to find situations where 1000+ iterations required
- ◆ Rigid impact zones: X. Provot, "Collision and self-collision handling in cloth model dedicated to design garment" Graphics Interface 1997
 - And Bridson Ph.D. thesis 2003
- ◆ When two regions collide, merge region and project velocities onto rigid or affine motions
- ◆ Efficiently resolves everything (but overdamped)
- ◆ Use as the last resort

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Additional repulsions

- ◆ Avoid alligator teeth problem - triangle locking - with three steps:
 - Apply soft repulsion forces (at level comparable to geometry approximation)
 - Detect collisions, apply impulses
 - Rigid impact zones

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Plasticity & Fracture

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Plasticity & Fracture

- ◆ If material deforms too much, becomes permanently deformed: plasticity
 - Yield condition: when permanent deformation starts happening ("if stress is large enough")
 - Elastic strain: deformation that can disappear in the absence of applied force
 - Plastic strain: permanent deformation accumulated since initial state
 - Total strain: total deformation since initial state
 - Plastic flow: when yield condition is met, how elastic strain is converted into plastic strain
- ◆ Fracture: if material deforms too much, breaks
 - Fracture condition: "if stress is large enough"

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For springs (1D)

- ◆ Go back to Terzopoulos and Fleischer
- ◆ Plasticity: change the rest length if the stress (tension) is too high
 - Maybe different yielding for compression and tension
 - Work hardening: make the yield condition more stringent as material plastically flows
 - Creep: let rest length settle towards current length at a given rate
- ◆ Fracture: break the spring if the stress is too high
 - Without plasticity: "brittle"
 - With plasticity first: "ductile"

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