

Notes

- ◆ Assignment 2 going okay?
 - Make sure you understand what needs to be done before the weekend
- ◆ Read Guendelman et al, "Nonconvex rigid bodies with stacking", SIGGRAPH'03
- ◆ Mistake last class: (forgot a transpose in calculating torque)

$$S^T F_{\text{ext}} = \sum_i \left(X^{*T} - x_i^{*T} \right) f_i$$

$$= \begin{pmatrix} \sum_i f_i \\ \sum_i (x_i - X) \times f_i \end{pmatrix}$$

$$= \begin{pmatrix} F \\ \tau \end{pmatrix}$$

cs533d-winter-2005 1

Inertia Tensor Simplified

- ◆ Reduce expense of calculating $I(t)$:

$$I(t) = \sum_i m_i (x_i - X)^{*T} (x_i - X)^*$$

$$= \sum_i m_i \left[(x_i - X)^T (x_i - X) \delta - (x_i - X)(x_i - X)^T \right]$$

- Now use $x_i - X = R p_i$ and use $R^T R = \delta$

$$I(t) = \sum_i m_i \left[p_i^T R^T R p_i \delta - R p_i p_i^T R^T \right]$$

$$= R \left(\underbrace{\sum_i m_i (p_i^T p_i \delta - p_i p_i^T)}_{I_{\text{body}}} \right) R^T$$

cs533d-winter-2005 2

Inertia Tensor Simplified 2

- ◆ So just compute inertia tensor once, for object space configuration
- ◆ Then $I(t) = R I_{\text{body}} R^T$
- ◆ And $I(t)^{-1} = R (I_{\text{body}})^{-1} R^T$
 - So precompute inverse too
- ◆ In fact, since I is symmetric, know we have an orthogonal eigenbasis Q
- ◆ Rotate object-space orientation by Q
 - Then I_{body} is just diagonal!

cs533d-winter-2005 3

Degenerate Inertia Tensors

- ◆ Inertia tensor can always be inverted unless all the points of the object line up (object is a rod)
 - Or there's only one point
- ◆ We don't care though, since we can't track rotation around that axis anyways
 - So diagonalize I , and only invert nonzero elements

cs533d-winter-2005 4

Taking the limit

- ◆ Letting our decomposition of the object into point masses go to infinity:
 - Instead of sum over particles, integral over object volume
 - Instead of particle mass, density at that point in space

$$\sum_i m_i \text{foo}(x_i) \rightarrow \iiint_x \rho(x) \text{foo}(x) dx$$

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Computing Inertia Tensors

- ◆ Do the integrals: $I_{\text{body}} = \iiint_p \rho (p^T p \delta - p p^T) dp$
- ◆ Lots of "fun"
- ◆ You *may* just want to look them up instead
 - E.g. Eric Weisstein's World of Science on the web
- ◆ If not... align axis perpendicular to planes of symmetry (of ρ) in object space
 - Guarantees some off-diagonal zeros
- ◆ Example: sphere, uniform density, radius R

$$\begin{pmatrix} \frac{2}{5} MR^2 & 0 & 0 \\ 0 & \frac{2}{5} MR^2 & 0 \\ 0 & 0 & \frac{2}{5} MR^2 \end{pmatrix}$$

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Approximating Inertia Tensors

- ◆ For complicated geometry, don't really need exact answer
- ◆ Could just take the inertia tensor from a simpler geometric figure (will anyone notice?)
- ◆ Or numerically approximate integral
 - If we can afford to spend a lot of time precomputing, life is simple
 - Grid approach: sample density...
 - Monte Carlo approach: random samples

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Combining Objects

- ◆ What if object is union of two simpler objects?
- ◆ Integrals are additive
 - But DO NOT USE $I_1(t)+I_2(t)$:
 - World-space formulas ($x-X$) use the X for the object: X_1 and X_2 may be different
 - Simplified I_{body} formula based on having centre of mass at origin
 - Let's work it out from the integral of $I(t)$
- ◆ Combined mass: $M=M_1+M_2$
- ◆ Centre of mass of combined object:

$$X = \frac{\int_{\Omega_1 \cup \Omega_2} \rho x}{\int_{\Omega_1 \cup \Omega_2} \rho} = \frac{M_1 X_1 + M_2 X_2}{M}$$

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Combined Inertia Tensor

$$\begin{aligned} I(t) &= \int_{\Omega_1 \cup \Omega_2} \rho(x-X)^{*T}(x-X)^* \\ &= \int_{\Omega_1} \rho(x-X_1+X_1-X)^{*T}(x-X_1+X_1-X)^* + \int_{\Omega_2} \dots \\ &= \int_{\Omega_1} \rho(x-X_1)^{*T}(x-X_1)^* + \int_{\Omega_1} \rho(X_1-X)^{*T}(x-X_1)^* \\ &\quad + \int_{\Omega_1} \rho(x-X_1)^{*T}(X_1-X)^* + \int_{\Omega_1} \rho(X_1-X)^{*T}(X_1-X)^* + \int_{\Omega_2} \dots \\ &= I_1(t) + (X_1-X)^{*T} \underbrace{\int_{\Omega_1} \rho(x-X_1)^*}_0 + \underbrace{\int_{\Omega_1} \rho(X_1-X)^{*T}(x-X_1)^*}_0 \\ &\quad + M_1(X_1-X)^{*T}(X_1-X)^* + \int_{\Omega_2} \dots \\ &= I_1(t) + M_1(X_1-X)^{*T}(X_1-X)^* + I_2(t) + M_2(X_2-X)^{*T}(X_2-X)^* \end{aligned}$$

cs533d-winter-2005 9

Numerical Integration

- ◆ Recall equations of motion

$$\frac{d}{dt} V = F/M \quad \frac{d}{dt} L = \tau$$

$$\frac{d}{dt} X = V \quad \omega = I(t)^{-1} L$$

$$\frac{d}{dt} R = \omega^* R$$
- ◆ X and V is just like particle motion
- ◆ Angular components trickier:
 - R must remain orthogonal, but standard integration will cause it to drift
 - Can use Gram-Schmidt, but expensive and biased

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Improving on R

- ◆ Instead of 9 numbers for 3 DOF, use a less redundant representation
- ◆ Euler angles: 3 numbers
 - But updating with angular velocity is painful
- ◆ Quaternions: 4 numbers

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What are quaternions?

- ◆ Instead of R , use $q=(s,x,y,z)$ with $|q|=1$
 - Can think of q as a "super complex number" $s+xi+yj+zk$
 - $i^2=j^2=k^2=-1$, $ij=-ji=k$, $jk=-kj=i$, $ki=-ik=j$
 - Quaternions don't commute! $q_1 q_2 \neq q_2 q_1$ in general
- ◆ Represents "half" a rotation:
 - $s=\cos(\theta/2)$
 - $|x,y,z|^2=\sin^2(\theta/2)$
 - Axis of rotation is (x,y,z)
- ◆ Conjugate (inverse for unit norm) is

$$\bar{q} = (s, -x, -y, -z)$$

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Rotating with quaternions

- ◆ Instead of Rp, calculate $q(0, p)\bar{q}$
- ◆ Composing a rotation of $\Delta t\omega$ to advance a time step:

$$q_{n+1} = \left(\cos\left|\Delta t \frac{\omega}{2}\right|, \sin\left|\Delta t \frac{\omega}{2}\right| \frac{\omega}{|\omega|} \right) q_n$$

- ∪ For small $\Delta t\omega$ approximate:

$$q_{n+1} = \left(1, \Delta t \frac{\omega}{2} \right) q_n = q_n + \Delta t \frac{(0, \omega)}{2} q_n$$

- ∪ From this get the differential equation:

$$\dot{q} = \frac{1}{2}(0, \omega)q$$

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Integrating Rotation

- ◆ Can update like Symplectic Euler, but need to renormalize q after each step
- ◆ For reasonable accuracy, limit time step according to rate of rotation
 - Don't try for more than a quarter turn per time step, say
 - Stability is not an issue due to renormalization
- ◆ For more accurate methods, see S. R. Buss, "Accurate and efficient simulation of rigid body rotations", JCP 2000

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Converting q to R

- ◆ Clearly superior to use quaternions for storing and updating orientation
- ◆ But, slightly faster to transform points with rotation matrix
- ◆ If you need to transform a lot of points (collision detection...) may want to convert q into R
- ◆ Basic idea: columns of R are rotated axes $R(1,0,0)^T$, $R(0,1,0)^T$, and $R(0,0,1)^T$
- ◆ Do the rotation with q instead.
 - Can simplify and optimize for the zeros - look it up

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Gravity

- ◆ Force on a point is $m_i g$
- ◆ Net force:

$$F = \sum_i m_i g = Mg$$
- ◆ Net torque: $\tau = \sum (x_i - X) \times m_i g$

$$= \left(\left(\sum_i m_i x_i \right) - MX \right) \times g$$

$$= 0$$

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Collision Impulses

- ◆ Can use same collision detection as deformable objects
 - Since geometry is fixed, may be cheaper
 - E.g. can use level set approximation to geometry
- ◆ But applying collision impulses is more complicated than for simple particles
 - Need to take into account angular motion too
- ◆ Use same principle though for the colliding points
 - What is the impulse that causes their relative velocity to change as desired?

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Frictionless impulse

- ◆ Object velocities at point:
 - $v_i = \omega_i \times (x - X_i) + V_i$
- ◆ Relative velocity $v = v_1 - v_2$
 - Normal component $v_n = v \cdot n$
- ◆ Want post-collision relative normal velocity to be $v_n^{after} = -\epsilon v_n$
- ∪ Apply an impulse $j = j_n n$ in the normal direction to achieve this

$$V_i^{after} = V_i + M_i^{-1} j_i$$

$$L_i^{after} = L_i + (x - X_i) \times j_i$$

$$\omega_i^{after} = \omega_i + I_i(t)^{-1} (x - X_i) \times j_i$$

$$j_i = (-1)^{i+1} j_n n$$

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Computing frictionless impulse

$$K_i = \frac{1}{M_i} \delta + (x - X_i)^{*T} I_i^{-1} (x - X_i)^{*}$$

$$j = \frac{-(1 + \epsilon)v_n}{n^T (K_1 + K_2)n} n$$

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Computing static friction

$$v^{after} = -\epsilon v_n n$$

$$j = (K_1 + K_2)^{-1} (-v - \epsilon v_n n)$$

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Computing sliding friction

$$T = \frac{v - v_n n}{|v - v_n n|}$$

$$j = j_n n - \mu j_n T$$

$$j_n = \frac{-(1 + \epsilon)v_n}{n^T (K_1 + K_2)(n - \mu T)}$$

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Computing friction

- ◆ Static friction valid only in “friction cone”

$$|j_T| \leq \mu |j_n|$$

- ◆ Approach:

- Calculate static friction impulse (whatever it takes to make relative velocity zero)
- Check if it's in the friction cone
- If so, we're done
- If not, try again with sliding

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Sliding friction

- ◆ If computed static friction impulse fails friction cone test
- ◆ We'll assume sliding direction stays constant during impact: tangential impulse just in the initial relative velocity direction
 - Not true in some situations...

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Rigid Collision Algorithms

- ◆ Use the same collision response algorithm as with particles
 - Identify colliding points as perhaps the deepest penetrating points, or the first points to collide
 - Make sure they are colliding, not separating!
- ◆ Problem: multiple contact points
 - Fixing one at a time can cause rattling.
 - Can fix by being more gentle in resolving contacts - negative coefficient of restitution
- ◆ Problem: multiple collisions (stacks)
 - Fixing one penetration causes others
 - Solve either by resolving simultaneously or enforcing order of resolution

cs533d-winter-2005 24