# Simulated Annealing for Profile and Fill Reduction of Sparse Matrices 

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## Summary

Simulated annealing can minimize both profile and fill of sparse matrices. We applied these techniques to a number of sparse matrices from the Harwell-Boeing Sparse Matrix Collection. We were able to reduce profile typically to about $80 \%$ of that attained by conventional profile minimization techniques (and sometimes much lower), but fill reduction was less successful ( $85 \%$ at best). We present a new algorithm that significantly speeds up profile computation during the annealing process. Simulated annealing is, however, still much more time-consuming than conventional techniques and is therefore likely to be useful only in situations where the same sparse matrix is being used repeatedly.

## 1 Introduction

Problems that require the solution of systems of linear equations of the form

$$
\begin{equation*}
\mathbf{A x}=\mathbf{b} \tag{1}
\end{equation*}
$$

where $\mathbf{A}$ is $N \times N,|\mathbf{x}|=|\mathbf{b}|=N$ occur frequently in many areas, often with a large value of $N$. Directly solving linear systems like (1) is, in general, an $O\left(N^{3}\right)$ process. Iterative methods can usually improve on this and, when they converge, are often preferred.

If $\mathbf{A}$ is sparse, however, iterative methods have less of an edge: direct solutions can often do much better than $O\left(N^{3}\right)$. The principal drawback when solving sparse systems directly is the "fill" created during the decomposition procedure: elements of $\mathbf{A}$ which were initially zero must become non-zero and therefore enter into the later stages of the decomposition.

The success of direct methods hinges on techniques to reduce fill by solving the equivalent problem

$$
\mathbf{A}^{\prime} \mathbf{x}^{\prime}=\mathbf{b}^{\prime}
$$

where $\mathbf{x}^{\prime}=\mathbf{P} \mathbf{x}, \mathbf{A}^{\prime}=\mathbf{P} \mathbf{A} \mathbf{P}^{T}, \mathbf{b}^{\prime}=\mathbf{P b}$, and $\mathbf{P}$ is a permutation of the rows and columns of the identity matrix $\mathbf{I}$ such that $\mathbf{P} \mathbf{P}^{T}=\mathbf{I}$. These techniques select a $\mathbf{P}$ that makes $\mathbf{A}^{\prime}$ better (according to some criterion) than $\mathbf{A}$. This amounts to a reordering of $\mathbf{A}$ into $\mathbf{A}^{\prime}$.

Finding an optimal $\mathbf{A}^{\prime}$ is an NP-hard problem: there are $N$ ! possible reorderings of $\mathbf{A}$ and no way to find the optimal one short of trying them all. The usual approach is to follow some heuristic procedure in reordering A such as: Reverse Cuthill-McKee (RCM), Minimum Degree Algorithm (MDA), Gibbs-King (GK), Nested Dissection (ND), etc.

All of these methods are capable of producing generally satisfactory results, but they all have their shortcomings. They might be dependent on the correct choice of a starting node (RCM) or an initial grouping
(ND). In any case, none of them makes any definite claims about minimizing fill.

What we'll explore in this paper is the application of a multivariate optimization technique called "simulated annealing" that can in principle be applied to any minimizant or maximizant in NP-hard problems. In particular, we'll investigate whether it can be practically applied to the minimizants of profile and fill to produce better orderings of A. Previous work in [1] looked at the minimizants of profile, wavefront, and bandwidth. We will compare our results with this work where they overlap.

## 2 Simulated Annealing

(Most of this section follows the presentation in [11], although [8] presented the original idea.)

The statistical behaviour of physical systems with large numbers of degrees of freedom inspired the simulated annealing technique.

To "anneal" is "to heat (glass, metals, etc.) and then cool slowly to prevent brittleness". This is just one instance of a fundamental observation about nature: given sufficient time and a mechanism to do so, a system will always tend to adjust itself to a minimal energy state. For instance

- The surface of a lake is flat.
- (Slowly) cooled liquids form highly-regular crystals.
- Air molecules spread evenly in a room.

All of these represent systems with large numbers of degrees of freedom achieving global minima.

Most iterative techniques that attempt to solve global optimization problems are, in a sense, "greedy": as soon as they find a better solution, they adopt it. For this reason, these techniques don't always behave well
in the presence of local minima.

How, then, are molecules able to "solve" the minimal energy problem globally? Because nature gives them sufficient time and energy to rearrange themselves in a way that ultimately satisfies the global minimum.

The Boltzmann distribution permits a system to exist in a state that is energy E above its minimum energy state with probability

$$
\begin{equation*}
P(E) \sim e^{\frac{-E}{k_{B} T}} \tag{2}
\end{equation*}
$$

where $T$ is the temperature and $k_{B}$ is Boltzmann's constant. This means that for all $T>0$ there's always a chance for a system stuck in a local minimum to acquire enough energy to move out of that minimum, but that as $T \rightarrow 0$, that probability becomes vanishingly small.
"Simulated" annealing (which we'll henceforth refer to as "SA") is then a computer simulation of physical annealing. Because it is a simulation, the minimizant can be any quantity we choose, not just energy.

The idea of sampling a simulation of a physical system which obeys a Boltzmann distribution originated in [10]. The development of SA as an optimization technique is due to [8].

In order to perform SA, we need (at least):

- an initial configuration for the system
- a set of "moves" (also known as "options"): distinct ways to randomly change the configuration. Each move should be reversible and it should be possible to reach any part of the configuration space in a finite number of moves.
- a minimizant (" $E$ "): what we're trying to minimize. It (or, more commonly, its increment) needs to be evaluated after the application of any move.
- a control parameter (" $T$ "): an indication of how willing we are at any given point to tolerate increases in the minimizant.
- an annealing schedule: analogous to the "cooling rate", this says how $T$ decreases as the simulation proceeds. The schedule also specifies how many attempts we perform at each temperature.

Given these things, the SA algorithm (in only slightly simplified form) proceeds as follows:

```
C\leftharpoonup initial configuration
T}\leftarrow\mathrm{ initial temperature
repeat
    repeat a specified number of times (according to annealing schedule)
        C'}\leftarrow\mathrm{ apply randomly-chosen move to C
        \deltaE}\leftarrowE(\mp@subsup{C}{}{\prime})-E(C
        if }\deltaE<0\mathrm{ or }\mp@subsup{e}{}{-\frac{\deltaE}{T}}>\operatorname{random}(0,1
            C\leftarrowC'
    T}\leftarrow\mathrm{ lower }T\mathrm{ according to annealing schedule
    until we can't find a lower E(C')
```

The idea is that we always change configuration if we move to a lower energy state, but that we sometimes change configuration even if we move to a higher state, although as the temperature drops this is less and less likely to happen.

The main drawbacks of SA are:

- Proofs that it converges to an optimal solution are hard to come by.
- There are only very rough guidelines in the appropriate choice of the initial $T$ and the annealing schedule. Often, they are chosen by trial-and-error.
- The algorithm needs to assess $E\left(C^{\prime}\right)$, the "energy" of the changed configuration, efficiently, since it is frequently needed.


## 3 Simulated Annealing and Sparse Matrices

How then do we use SA in sparse matrix problems? We can apply the algorithm given above if we can provide its required inputs.

In all further discussion, we will restrict ourselves to the case of symmetric matrices. This is purely for our own convenience: there is no reason why SA shouldn't work as well with non-symmetric matrices as it does with symmetric ones.

We have implemented a system in C on a Sun SPARCStation-2 that is capable of performing SA profile or fill reduction on an arbitrary symmetric matrix. Hereafter, we'll refer to the two procedures as SAPR (Simulated Annealing Profile Reduction) and SAFR (Simulated Annealing Fill Reduction).

Here follow the design choices affecting SA computation.

### 3.1 Initial Configuration

This is just a representation of the sparse matrix itself. In our case, allocating an array of nodes, each with a dynamically-sized array of adjacencies is advantageous. This takes up slightly more space than the usual double-array storage scheme (described in [6]), but its dynamic nature allows us to add adjacencies as they occur during fill.

### 3.2 Moves

One move that immediately suggests itself is to exchange two randomly-chosen rows (and the corresponding columns, since we're dealing with a symmetric matrix). We'll call this a "swap".

We'll discuss the impact of swaps on evaluations of the minimizant when we discuss the individual minimizants later.

### 3.3 Minimizant

We can choose this as needed. For this investigation, we'll take it to be either profile or fill. We'll talk about the practical limitations of this below. We could also have chosen bandwidth, as was done by [1], but bandwidth is a less reliable indicator of fill than profile.

### 3.4 Control Parameter and Annealing Schedule

The easiest way to think of "temperature" in this context is to recall that in analogy with (2), a configuration change that increases the minimizant by an amount equal to $T$ will be accepted $63 \%\left(=1-e^{-1}\right)$ of the time. (We take $k_{B}=1$ in this analogy.)

We want the system to be initially "hot": increases in the minimizant are almost as likely to be accepted as decreases. This is a tradeoff we make. If we start out with a $T$ that is too low, we may miss global minima. On the other hand, if we start out with a $T$ that is too high, we waste computing time randomly changing the system configuration. In most initial SA investigations, it's prudent to overestimate $T$ until the researcher acquires some familiarity with the problem. This will be our approach:

$$
T_{\text {initial }}(\mathbf{A})=10 \frac{\{\text { initial profile of } \mathbf{A}\}}{N}
$$

This heuristic formula makes $T$ large when we deal with a matrix that has a large profile, but the $N^{-1}$ factor prevents it from getting large as the size of the matrix itself increases.

We'll also follow a common (naive) approach to an annealing schedule. We are given two dimensionless parameters: $F_{T}$ and $A_{T}$. At any given temperature, we try a maximum of $N A_{T}$ swaps. If no successful reductions of the minimizant have occurred after this, we assume we can't find a lower $E\left(C^{\prime}\right)$ and stop. Otherwise, we lower the temperature by a factor of $F_{T}$ and iterate. In addition, if at any temperature we ever have $N\left(1+0.1 A_{T}\right)$ successes, we take this to indicate that the temperature is too high and lower the temperature early. Typically, $F_{T}=0.9$ and $A_{T}=100$, but we'll consider others.

## 4 SAPR: Simulated Annealing Profile Reduction

It would be possible to compute the profile of the matrix a priori after each swap, but this is inefficient, being $O(N-\min (i, j))=O(N)$ for the storage scheme being used. Instead, we can note that swapping row $i$ with row $j: j>i$ affects only the areas of the matrix shown in gray in Figure 1. Arrows indicate which elements are being effectively exchanged by the swap.

Only individual row profiles of rows whose indices are greater than or equal to $i$ can be affected. Also, the gray areas are themselves sparse (in general) so we can efficiently compute changes to the individual row profiles by traversing the adjacency arrays of the affected nodes of the matrix.

The overall change in profile as a result of a swap can therefore be computed in $O\left(B_{h}\right)$ (integer operations) where $B_{h}$ is the (mean) half-bandwidth of the matrix.

| ordering | profile |
| :--- | ---: |
| Original | 32 |
| Reverse Cuthill-McKee | 18 |
| SAPR | 17 |

Table 1: Results of Profile Minimization on Figure 2

### 4.1 A Simple Example

We first present a small example: a sparse matrix whose graph is shown in Figure 2. (This was originally used as an example in [6].)

Figures 3 and 4 show the sparsity patterns before and after RCM-ordering of this matrix. (All examples of RCM in this paper start from a pseudoperipheral node using the algorithm given in [6].) In this and all of the other sparsity diagrams we show, the original elements of the matrix are in black and those that would be created by fill are in gray.

Figure 5 and Table 1 show the results of SAPR on this matrix. The difference between SAPR and RCM is quite small ( $=1$ ) in this case, but at least it demonstrates that SAPR can find a better solution.

### 4.2 A 2-D Grid

Figures 6 and 7 show a more realistic example: a $100 \times 100$ array corresponding to a 2 -dimensional, 5 -point PDE problem on a $10 \times 10$ grid.

Figure 8 and Table 2 show the results of SAPR on this matrix. It's important to note the times involved: on a Sun SPARCstation-2 RCM required less than a second to run, while SAPR took about 15 minutes.

| ordering | profile |
| :--- | ---: |
| Original | 909 |
| Reverse Cuthill-McKee | 829 |
| SA Profile Reduction | 812 |

Table 2: Results of Profile Minimization of $100 \times 1002$-D 5-point PDE solution matrix

This suggests that any practical application of SAPR seeking to minimize the amount of CPU time used should take into account both profile reduction and solution time. Of course, if the same matrix is being used many times, the SAPR cost can be amortized and the (presumed) reduction in solution time for each use may more easily make up the difference.
$f_{S A P R}$ is the improvement ratio of SAPR compared to the best non-SA-obtained profile reported in our sources. If we examine $f_{S A P R}$ for a wide range of $N$, we get the results shown in Figure 9: as $N$ increases, the solution gets (almost) monotonically worse, but not dramatically so.

### 4.3 The Harwell-Boeing Sparse Matrix Collection

To examine how SAPR does on a wider range of matrices, we will apply it to a subset of matrices from the Harwell-Boeing Sparse Matrix collection (see [4]).

Tables 6-10 show the results of SAPR on a subset of the matrices in the Harwell-Boeing test set (description in [4]). Table 11 is the key to these tables.

Taken overall, there's a wide variation of $f_{S A P R}$. There's an improvement in the majority of cases ( 71 out of 95 ), but in some cases (e.g. HB\#13/NOS2) there's no improvement at all! How can we account for this?

Figure 10 plots $f_{S A P R}$ as a function of $N$ for all the matrices in the subset. There is no obvious correlation
between the two: SAPR appears to be as likely to be successful with a small matrix as with a large one. The near-monotonic increase in $f_{S A P R}$ we observed for a single class of problem in Figure 9 is not evident here. Perhaps some other attribute correlates better with $f_{S A P R}$. Figure 11 plots $f_{S A P R}$ against the original source of the matrix, as reported in [4]. The abscissa is arranged in increasing order of mean $f_{S A P R}$ for all matrices within the given source. Figure 11 also shows the discipline the matrices in each source came from. Performance for structural engineering and finite element matrices appears widespread. The single 9-point $30 \times 30$ PDE appears close to $f_{S A P R}=1$, as we might have expected from the 5 -point PDE results shown above in Figure 9. All the electric power matrices have low $f_{S A P R}$ 's.

Nevertheless, even within a given discipline, there can be a wide spread of $f_{S A P R}$. Could this be the result of the annealing schedule?

### 4.4 Altering the Annealing Schedule

There's no guarantee that the annealing schedule we've used for all our work so far is optimal. Let's choose a subset of the matrices we've been using and see what happens when we change the schedule.

The subset we'll choose correspond to Harwell-Boeing Tape File \#7 (hereafter "HBTF \#7"). We have several reasons for selecting these:

- They arise from a common problem domain: finite element modelling.
- They show a wide range in $f_{S A P R}$, from 0.576 to 1.541 .
- They correspond to the same matrices used in [1], so we can compare our results and timings.

We'll perform SAPR on all 30 matrices in HBTF \#7 with the five different annealing schedules S1-5 described in Table 3. S1 is identical to the schedule used for Tables 6-10. The other schedules vary $F_{T}$ and $A_{T}$.

| Schedule Name | $F_{T}$ | $A_{T}$ | RCMP used? |
| :---: | :---: | :---: | :---: |
| S1 | 0.90 | 100 | no |
| S2 | 0.95 | 50 | no |
| S3 | 0.95 | 100 | no |
| S4 | 0.90 | 50 | no |
| S5 | 0.90 | 100 | yes |

Table 3: SAPR Schedule Specifications

S5 is special. Before starting SA, the matrix is preordered with the RCM algorithm. We refer to this as "RCM Preconditioning" (hereafter, "RCMP").

We do not propose this as an improvement to SAPR: since we're supposed to start with a "hot" matrix, its initial configuration should not matter. What we can do, though, is use it as an indicator of how sensitive SAPR is to the annealing schedule. If two values of $f_{S A P R}$ with and without RCMP differ greatly, we take it to be an indication that our schedule is sub-optimal.

Tables $12-13$ show the results ${ }^{1}$. Table 14 is the key to these tables. It is interesting to note that while no single schedule outperforms the others, the most rapidly-cooled, least iterated one, S 4 , is with one exception always worse than the rest.

### 4.5 Comparison With Previous Work

As mentioned above, we can compare our results for HBTF \#7 not only with those of the minimal non-SA profiles, but also with the previous SAPR work done by Armstrong in [1]. Tables 15-16 show this. Table 17

[^0]is the key to these tables.

Varying annealing schedules and using minimal profiles has improved our results. Now we have uniformly lower profiles than non-SA methods, except in the one small case (DWT 66) for which we suggest that both GK and SAPR find the minimal profile.

In all but one case (DWT 2680 - the largest matrix in HBTF \#7), we also find lower profiles than Armstrong. This is something of a surprise, as he chose a somewhat more elaborate annealing schedule with a parameterization that varied matrix-by-matrix.

Nevertheless, it is safe to conclude that we have found no clear heuristic on choosing an annealing schedule for profile redution. One must simply try a number of points in the schedule parameter space. (This conclusion is often reached in SA problems.)

Armstrong also cites timing results: The total CPU time required for SAPR profiles of all 30 matrices was 600 hours on a DEC 20/60 mainframe. The total CPU time for our SAPR results for the same 30 matrices in Tables $15-16$ was 10.1 hours on a SPARCStation $4 / 690$ server. Certainly, a large part of the difference is attributable to the difference in hardware technology, but it is likely that our profile increment computation speedup also contributed.

## 5 SAFR: Simulated Annealing Fill Reduction

It is conceptually easy in SA to switch minimizants from profile to fill. Problems arise, however, in computing the change in fill as a result of a swap, which SA requires frequently.

Since a single swap of rows $i$ and $j$ can introduce a large amount of fill that cascades into all rows $k>$ $\min (i, j)$, fill increment computation is much more expensive than profile increment computation. It would

| ordering | fill |
| :--- | ---: |
| Original | 15 |
| Reverse Cuthill-McKee | 3 |
| SAFR | 2 |

Table 4: Results of Fill Minimization on Figure 2
be extremely useful to try to find a cheaper way of computing the fill increment.

We'll investigate fill vs. profile increment computation in greater detail below.

### 5.1 A Simple Example

We can perform SAFR on the same simple example shown in Figure 2. Figure 12 and Table 4 show the results.

Again, an insignificant improvement (=1) in fill over RCM, but, again, this is just an illustration of the feasibility of the technique.

### 5.2 A 2-D Grid

We again use the more realistic example of Figure 6. Figure 8 and Table 5 show the fill minimization results. The table also includes the profile minimization results by way of illustrating something suggested by a comparison of Figures 8 and 13: orderings which minimize fill can be quite distinct from those which minimize profile.

| ordering | profile | fill |
| :--- | ---: | ---: |
| Original | 909 | 720 |
| Reverse Cuthill-McKee | 829 | 640 |
| SAPR | 812 | 623 |
| SAFR | 3123 | 400 |

Table 5: Results of Minimization of $100 \times 1002$-D 5-point PDE solution matrix

### 5.3 Time Requirements of Profile vs. Fill Computation

The 2-D, 5-point grid is a scaleable problem that allows us to see how fill and profile increment computations scale with the size of the problem. Figure 14 shows this for a wide range of $N$. Note that while both curves are steeper than $O(N)$, the fill curve is much steeper than the profile curve. For this reason, we can only do fill minimization on small matrices.

### 5.4 The Harwell-Boeing Sparse Matrix Collection

Table 18 shows the results of SAFR on a small subset of the matrices in the Harwell-Boeing test set. Most of them were chosen from those members of the subset we used for SAPR which had $N<100$. Two additional matrices, 685 BUS and 1138 BUS, were chosen to include results from the tie-breaking minimum degree results presented in by Cavers in [2]. Table 19 is the key to these tables.

All of the matrices underwent SAFR with default schedule S 1 except for the two large matrices, which used RCMP combined with the initial assumption of $T=1$ (a very cool system) to get these numbers in a reasonable length of time ${ }^{2}$.

[^1]SAFR was able to improve over the minimum degree algorithm (or Cavers' enhancement of it) in 8 out of 15 cases, and only did significantly worse in the one largest case.

The times to produce conventional fill results were never more than a few seconds.

## 6 Conclusions and Further Work

SA has potentially wide application in direct sparse matrix solution. Although SAPR takes considerably longer than RCM or GK (and probably all the others), it can produce a significant reduction in profile for a wide spectrum of matrix types. SAFR, on the other hand, takes a considerably longer time than either ND or MDA, and reduces fill less dramatically than SAPR reduces profile.

SA is particularly applicable in two areas:

- situations where the same matrix $\mathbf{A}$ is used repeatedly

Then, the additional cost of SA would be amortized over a large number of solutions.

- when validating other, faster algorithms for profile and fill reduction
(This was pointed out in [1].) Given the optimal annealing schedule (which we do not claim to have used here), it should be possible to determine what the actual minimum value of the minimizant is.

Possibilities for additional work include:

- More work needs to be done on heuristics for choosing an appropriate annealing schedule.
- There may be some way to improve fill increment computation so that SAFR will be practical on large matrices.
- SA should lend itself well to nested dissection, as it has been used in analogous applications for reducing interconnectivity in VLSI layout (see [8] and [12]).


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## References

[1] B. Armstrong, 'Near-Minimal Matrix Profiles and Wavfronts for Testing Nodal Resequencing Algorithms', Int. j. numer. methods eng., 21, 1785-1790 (1985).
[2] I. A. Cavers, Using Deficiency Measure for Tiebreaking the Minimum Degree Algorithm, Techical Report 89-2, Department of Computer Science, University of British Columbia, 1989.
[3] I. A. Cavers, work in progress.
[4] I. S. Duff, R. G. Grimes, J. G. Lewis, and B. Poole, 'User's Guide for the Harwell-Boeing Sparse Matrix Collection', ACM SIGNUM Newsletter, 17 (1982), p. 22.
[5] G. C. Everstine, 'A Comparison of Three Resequencing Algorithms for the Reduction of Matrix Profile and Wavefront', Int. j. numer. methods eng., 14, 837-853 (1979).
[6] J. A. George and Joseph W-H. Liu, Computer Solution of Large Sparse Positive Definite Systems, Prentice-Hall, New Jersey, 1981.
[7] J. A. George and Joseph W-H. Liu, User Guide for SPARSPAK: Waterloo Sparse Linear Equations Package, Research Report CS-78-30, Department of Computer Science, University of Waterloo, 1978.
[8] S. Kirkpatrick, C. D. Gelatt, Jr., and M. P. Vecchi, 'Optimization by Simulated Annealing', Science, 220 (1983), pps. 671-680.
[9] J. G. Lewis, 'Implementation of Gibbs-Poole-Stockmeyer and Gibbs-King Algorithms', ACM Trans. on Math. Softw., 8 (2) (1982), pps. 180-189.
[10] N. Metropolis, A. Rosenbluth, M. Rosenbluth, A. Teller, and E. Teller, 'Equation of State Calculations by Fast Computing Machines', J. Chem. Phys., 21 (1953), pps. 1087-1092.
[11] W. H. Press, B. P. Flannery, S. A. Teukolsky, and W. T. Vetterling, Numerical Recipes, Cambridge University Press, New York, 1988.
[12] M. P. Vecchi and S. Kirkpatrick, 'Global Wiring by Simulated Annealing', IEEE Trans. on CAD, CAD-2 (1983), pps. 215-222.

| $\begin{gathered} \text { H-B } \\ \# \end{gathered}$ | Matrix <br> Name | $N$ | \# of <br> Matrix <br> Nonzeros | Conventional <br> Profiles |  | Simulated <br> Annealing |  | $f_{S A P R}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | RCM | GK | Profile | Time |  |
| 3 | ASH292 | 292 | 1250 | 3738 | 3479 | 2694 | 457 | 0.774 |
|  | ASH85 | 85 | 304 | 617 | 564 | 491 | 91 | 0.871 |
| 4 | BCSPWR01 | 39 | 85 | 99 | 100 | 83 | 19 | 0.838 |
|  | BCSPWR02 | 49 | 108 | 214 | 180 | 113 | 24 | 0.628 |
|  | BCSPWR03 | 118 | 297 | 774 | 644 | 478 | 87 | 0.742 |
|  | BCSPWR04 | 274 | 943 | 4331 | 3609 | 2224 | 316 | 0.616 |
|  | BCSPWR05 | 443 | 1033 | 10784 | 7305 | 3015 | 420 | 0.413 |
|  | BCSPWR06 | 1454 | 3377 | 63182 | 48265 | 17570 | 1940 | 0.364 |
|  | BCSPWR07 | 1612 | 3718 | 74344 | 56119 | 21147 | 2400* | 0.377 |
|  | BCSPWR08 | 1624 | 3837 | 78187 | 57242 | 24741 | 2490* | 0.432 |
|  | BCSPWR09 | 1723 | 4117 | 79260 | 64788 | 26793 | 2300* | 0.414 |
| 5 | BCSSTK01 | 48 | 224 | 667 | 544 | 468 | 44 | 0.860 |
|  | BCSSTK02 | 66 | 2211 | 2145 | 2145 | 2145 | 3 | 1.000 |
|  | BCSSTK03 | 112 | 376 | 272 | 272 | 306 | 101 | 1.125 |
|  | BCSSTK04 | 132 | 1890 | 3965 | 3228 | 3162 | 1060 | 0.980 |
|  | BCSSTK05 | 153 | 1288 | 2254 | 2226 | 2194 | 464 | 0.986 |
|  | BCSSTK06 | 420 | 4140 | 13226 | 13723 | 12975 | 2980 | 0.981 |
|  | BCSSTK07 | 420 | 4140 | 13226 | 13723 | 12975 | 2980 | 0.981 |
|  | BCSSTK09 | 1083 | 9760 | 75581 | 66281 | 57194 | 9250 | 0.863 |
|  | BCSSTK10 | 1086 | 11578 | 19943 | 19685 | 28488 | 13300 | 1.447 |
|  | BCSSTK11 | 1473 | 17857 | 73117 | 66919 | 62103 | 20400 | 0.928 |

Table 6: Results of Profile Reduction of Harwell-Boeing Matrices

| $\begin{gathered} \mathrm{H}-\mathrm{B} \\ \# \end{gathered}$ | Matrix <br> Name | $N$ | \# of <br> Matrix <br> Nonzeros | Conventional <br> Profiles |  | Simulated <br> Annealing |  | $f_{S A P R}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | RCM | GK | Profile | Time |  |
| 5 | BCSSTK12 | 1473 | 17857 | 73117 | 66919 | 62103 | 20400 | 0.928 |
|  | BCSSTM10 | 1086 | 11589 | 19790 | 19685 | 28424 | 12300 | 1.444 |
| 6 | CAN 24 | 24 | 92 | 97 | 98 | 95 | 16 | 0.979 |
|  | CAN 61 | 61 | 309 | 408 | 367 | 340 | 85 | 0.926 |
|  | CAN 62 | 62 | 140 | 269 | 254 | 178 | 32 | 0.701 |
|  | CAN 73 | 73 | 225 | 774 | 699 | 524 | 52 | 0.750 |
|  | CAN 96 | 96 | 432 | 1234 | 1114 | 1078 | 123 | 0.968 |
|  | CAN 144 | 144 | 720 | 1074 | 979 | 972 | 227 | 0.993 |
|  | CAN 161 | 161 | 769 | 2610 | 2610 | 2473 | 238 | 0.948 |
|  | CAN 187 | 187 | 839 | 2374 | 2231 | 2163 | 294 | 0.970 |
|  | CAN 229 | 229 | 1003 | 4475 | 4423 | 3890 | 326 | 0.879 |
|  | CAN 256 | 256 | 1586 | 7977 | 6845 | 4166 | 650 | 0.609 |
|  | CAN 268 | 268 | 1675 | 7732 | 9665 | 4637 | 749 | 0.600 |
|  | CAN 292 | 292 | 1416 | 9275 | 8014 | 4057 | 545 | 0.506 |
|  | CAN 445 | 445 | 2127 | 20234 | 18786 | 14448 | 948 | 0.769 |
|  | CAN 634 | 634 | 3931 | 35131 | 32155 | 26111 | 2470 | 0.812 |
|  | CAN 715 | 715 | 3690 | 38449 | 35451 | 20722 | 2390 | 0.585 |
| 7 | DWT 59 | 59 | 163 | 255 | 255 | 214 | 35 | 0.839 |
|  | DWT 66 | 66 | 193 | 151 | 127 | 127 | 47 | 1.000 |
|  | DWT 72 | 72 | 147 | 297 | 255 | 147 | 33 | 0.576 |
|  | DWT 87 | 87 | 314 | 609 | 595 | 428 | 84 | 0.719 |

Table 7: Results of Profile Reduction of Harwell-Boeing Matrices (continued)

| $\begin{gathered} \mathrm{H}-\mathrm{B} \\ \# \end{gathered}$ | Matrix <br> Name | $N$ | \# of <br> Matrix <br> Nonzeros | Conventional <br> Profiles |  | Simulated <br> Annealing |  | $f_{S A P R}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | RCM | GK | Profile | Time |  |
| 7 | DWT 162 | 162 | 672 | 1479 | 1417 | 1117 | 216 | 0.788 |
|  | DWT 193 | 193 | 1843 | 5312 | 4416 | 4225 | 911 | 0.957 |
|  | DWT 198 | 198 | 795 | 1219 | 1115 | 1096 | 281 | 0.983 |
|  | DWT 209 | 209 | 976 | 3610 | 3823 | 2494 | 325 | 0.691 |
|  | DWT 221 | 221 | 925 | 2004 | 2002 | 2204 | 316 | 1.101 |
|  | DWT 234 | 234 | 534 | 1305 | 1115 | 814 | 173 | 0.730 |
|  | DWT 245 | 245 | 853 | 5196 | 3568 | 1939 | 271 | 0.543 |
|  | DWT 307 | 307 | 1415 | 8336 | 8540 | 6290 | 526 | 0.755 |
|  | DWT 310 | 310 | 1379 | 2836 | 2697 | 2639 | 541 | 0.878 |
|  | DWT 346 | 346 | 1786 | 7688 | 7335 | 5925 | 740 | 0.808 |
|  | DWT 361 | 361 | 1657 | 4714 | 4699 | 4646 | 647 | 0.989 |
|  | DWT 419 | 419 | 1991 | 8230 | 7654 | 6173 | 838 | 0.807 |
|  | DWT 492 | 492 | 1824 | 6575 | 5021 | 3156 | 716 | 0.629 |
|  | DWT 503 | 503 | 3265 | 14816 | 14539 | 11817 | 1930 | 0.813 |
|  | DWT 512 | 512 | 2007 | 4807 | 4456 | 4031 | 864 | 0.905 |
|  | DWT 592 | 592 | 2848 | 10848 | 10333 | 8940 | 1510 | 0.865 |
|  | DWT 607 | 607 | 2869 | 17261 | 14283 | 13013 | 1400 | 0.911 |
|  | DWT 758 | 758 | 3376 | 7822 | 7417 | 11433 | 1830 | 1.541 |
|  | DWT 869 | 869 | 4077 | 18424 | 14589 | 15820 | 2600 | 1.084 |
|  | DWT 878 | 878 | 4163 | 21513 | 18818 | 17499 | 2860 | 0.930 |
|  | DWT 918 | 918 | 4151 | 22187 | 19580 | 15286 | 2630 | 0.781 |

Table 8: Results of Profile Reduction of Harwell-Boeing Matrices (continued)

| $\begin{gathered} \text { H-B } \\ \# \end{gathered}$ | Matrix <br> Name | $N$ | \# of <br> Matrix <br> Nonzeros | Conventional <br> Profiles |  | Simulated <br> Annealing |  | $f_{S A P R}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | RCM | GK | Profile | Time |  |
| 11 | LSHP 265 | 265 | 1009 | 3479 | 3355 | 3168 | 169 | 0.944 |
|  | LSHP 406 | 406 | 1561 | 6541 | 6346 | 5970 | 329 | 0.941 |
|  | LSHP 577 | 577 | 2233 | 11012 | 10730 | 10113 | 570 | 0.942 |
|  | LSHP 778 | 778 | 3025 | 17158 | 16773 | 15893 | 854* | 0.948 |
|  | LSHP1009 | 1009 | 3937 | 25245 | 24741 | 23501 | 1300* | 0.950 |
|  | LSHP1270 | 1270 | 4969 | 35539 | 34900 | 33419 | 1750* | 0.958 |
|  | LSHP1561 | 1561 | 6121 | 48306 | 47516 | 46133 | 2170* | 0.971 |
|  | LSHP1882 | 1882 | 7393 | 63812 | 62855 | 61523 | 2810* | 0.979 |
|  | LSHP2233 | 2233 | 8785 | 82323 | 81183 | 90032 | 3290* | 1.109 |
|  | LSHP2614 | 2614 | 10297 | 104105 | 102766 | 102100 | 3890* | 0.994 |
|  | LSHP3025 | 3025 | 11929 | 129424 | 127870 | 124753 | 4610* | 0.976 |
| 13 | NOS1 | 237 | 627 | 467 | 468 | 872 | 82 | 1.867 |
|  | NOS2 | 957 | 2547 | 1907 | 1908 | 3937 | 506 | 2.064 |
|  | NOS3 | 960 | 8402 | 47536 | 41273 | 36487 | 3970 | 0.884 |
|  | NOS4 | 100 | 347 | 744 | 750 | 652 | 40 | 0.876 |
|  | NOS5 | 468 | 2820 | 25228 | 22471 | 19997 | 717 | 0.890 |
|  | NOS6 | 675 | 1965 | 9305 | 9095 | 12501 | 443 | 1.374 |
|  | NOS7 | 729 | 2673 | 34110 | 34110 | 34201 | 732 | 1.003 |
| 19 | GR. 30.30 | 900 | 4322 | 33872 | 28251 | 27170 | 1690* | 0.962 |
| 20 | PLAT362 | 362 | 3074 | 9261 | 13388 | 8238 | 1050 | 0.890 |
| 23 | BLCKHOLE | 2132 | 8502 | 171437 | 169219 | 107710 | 3210 | 0.637 |

Table 9: Results of Profile Reduction of Harwell-Boeing Matrices (continued)

| $\begin{gathered} \text { H-B } \\ \# \end{gathered}$ | Matrix <br> Name |  | \# of <br> Matrix | Conventional <br> Profiles |  | Simulated <br> Annealing |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $N$ | Nonzeros | RCM | GK | Profile | Time | $f_{S A P R}$ |
| 23 | SSTMODEL | 3345 | 13047 | 105421 | 104562 | 82805 | 6030 | 0.792 |
| 24 | BCSSTK19 | 817 | 3835 | 9594 | 8152 | 9505 | 1120 | 1.166 |
|  | BCSSTK20 | 485 | 1810 | 5069 | 4408 | 3859 | 336 | 0.875 |
|  | BCSSTK21 | 3600 | 15100 | 174478 | 172754 | 272798 | 6820 | 1.579 |
|  | BCSSTK22 | 138 | 417 | 851 | 842 | 729 | 63 | 0.866 |
| 28 | 494 BUS | 494 | 1080 | 13272 | 8412 | 2921 | 446 | 0.347 |
|  | 662 BUS | 662 | 1568 | 28727 | 16601 | 6847 | 720 | 0.412 |
|  | 685 BUS | 685 | 1967 | 25606 | 16314 | 6857 | 897 | 0.420 |
|  | 1138 BUS | 1138 | 2596 | 43680 | 36707 | 12278 | 1450 | 0.334 |
| 29 | ZENIOS | 2873 | 15302 | 12981 | 12723 | 23172 | 12100* | 1.821 |
| 30 | BCSSTK26 | 1922 | 16129 | 194842 | 188032 | 102187 | 17900 | 0.543 |

Table 10: Results of Profile Reduction of Harwell-Boeing Matrices (continued)

| Column | Description |
| :--- | :--- |
| H-B \# | Harwell-Boeing "Tape File Number" |
| Matrix Name | Harwell-Boeing designation of the matrix |
| $N$ | dimension of the matrix is $N \times N$ |
| \# of Matrix Nonzeros | number of non-zero elements in the matrix |
| RCM | Reverse Cuthill-McKee profile derived from <br> SPARSPAK library (source: [3]) |
| GK | Gibbs-King profile (source: [9]) |
| Profile | the SAPR result |
| Time | Sotal (user + system) CPU time (sec) required on a <br> ratio of Profile (with no RCMP) to the minimum <br> of RCM and GK |
| $f_{S A P R}$ | flags certain SA profile computations that did not converge <br> after 100 or more temperature decrements (all profile changes <br> were < $0.1 \%$ at that point, so this should not noticeably <br> affect overall results) |
| * |  |

Table 11: Key to Tables 6-10

| Matrix | Simulated Annealing Schedule |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | S1 |  | S2 |  | S3 |  | S4 |  | S5 |  |
| Name | Profile | Time | Profile | Time | Profile | Time | Profile | Time | Profile | Time |
| DWT 59 | 214 | 19.6 | 215 | 21.1 | 215 | 40.7 | 215 | 9.8 | 215 | 19.2 |
| DWT 66 | 127 | 26.6 | 127 | 24.4 | 127 | 50.6 | 204 | 12.8 | 127 | 26.0 |
| DWT 72 | 147 | 17.8 | 155 | 17.4 | 153 | 35.0 | 163 | 8.7 | 151 | 18.5 |
| DWT 87 | 428 | 50.4 | 428 | 47.8 | 429 | 90.1 | 462 | 22.5 | 431 | 49.2 |
| DWT 162 | 1117 | 127.0 | 1183 | 131.0 | 1258 | 234.8 | 1262 | 60.1 | 1110 | 131.4 |
| DWT 193 | 4225 | 536.5 | 4233 | 535.8 | 4230 | 1045.0 | 4228 | 254.5 | 4217 | 543.0 |
| DWT 198 | 1096 | 165.7 | 1094 | 172.8 | 1091 | 323.8 | 1094 | 79.8 | 1090 | 158.1 |
| DWT 209 | 2494 | 193.1 | 2493 | 199.9 | 3029 | 371.4 | 2503 | 96.6 | 2503 | 194.2 |
| DWT 221 | 2204 | 185.4 | 1643 | 197.8 | 1634 | 364.9 | 1650 | 92.9 | 2062 | 178.2 |
| DWT 234 | 814 | 95.3 | 818 | 94.1 | 815 | 172.8 | 838 | 45.7 | 818 | 88.6 |
| DWT 245 | 1939 | 153.9 | 2022 | 144.7 | 2041 | 297.4 | 1986 | 76.8 | 2024 | 157.2 |
| DWT 307 | 6290 | 304.5 | 6569 | 318.0 | 6315 | 627.2 | 6437 | 169.2 | 6391 | 310.1 |
| DWT 310 | 2639 | 302.5 | 2636 | 311.3 | 2631 | 603.5 | 2642 | 171.3 | 2645 | 320.6 |
| DWT 346 | 5925 | 457.8 | 5843 | 475.2 | 5882 | 863.5 | 5945 | 231.6 | 5842 | 446.2 |
| DWT 361 | 4646 | 377.8 | 4647 | 377.8 | 4638 | 773.1 | 4681 | 194.9 | 4642 | 381.5 |
| DWT 419 | 6173 | 509.7 | 6345 | 490.3 | 6147 | 1034.5 | 6309 | 255.8 | 6242 | 483.2 |
| DWT 492 | 3156 | 427.7 | 3466 | 439.5 | 2855 | 902.4 | 4663 | 239.7 | 3083 | 451.0 |
| DWT 503 | 11817 | 1180.6 | 11599 | 1079.6 | 11682 | 2167.8 | 11827 | 554.6 | 11611 | 1099.4 |
| DWT 512 | 4031 | 495.0 | 3918 | 438.5 | 3937 | 908.0 | 4325 | 219.8 | 3991 | 532.6 |
| DWT 592 | 8940 | 841.4 | 8914 | 805.6 | 10414 | 1535.2 | 9068 | 461.2 | 8933 | 884.0 |

Table 12: SAPR Results For HBTF \#7 With Several Annealing Schedules

| Matrix <br> Name | S1 |  | Simulated Annealing Schedule |  |  |  |  |  | S5 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | S2 |  | S3 |  | S4 |  |  |  |
|  | Profile | Time | Profile | Time | Profile | Time | Profile | Time | Profile | Time |
| DWT 607 | 13013 | 772.2 | 12700 | 773.2 | 12613 | 1428.6 | 13108 | 396.8 | 13075 | 820.7 |
| DWT 758 | 11433 | 953.2 | 9886 | 945.6 | 10020 | 1798.0 | 11342 | 541.0 | 7111 | 1409.6 |
| DWT 869 | 15820 | 1363.6 | 18164 | 1124.7 | 12416 | 2275.1 | 11723 | 701.8 | 12274 | 1307.9 |
| DWT 878 | 17499 | 1472.7 | 17733 | 1225.2 | 17638 | 2367.3 | 18262 | 702.2 | 17953 | $>1602.8$ |
| DWT 918 | 15286 | 1394.2 | 19452 | 1368.3 | 21280 | 2400.9 | 28358 | 694.0 | 15572 | 1392.7 |
| DWT 992 | 32204 | 4048.5 | 32258 | 3919.7 | 31940 | 7637.3 | 32526 | 2134.0 | 32794 | 4099.3 |
| DWT 1005 | 32213 | $>1504.4$ | 33116 | 1502.9 | 32167 | 2816.1 | 33189 | 810.5 | 32584 | 1604.5 |
| DWT 1007 | 19246 | 1811.2 | 19362 | 1455.2 | 16965 | 2805.7 | 20791 | 856.5 | 19288 | 1721.4 |
| DWT 1242 | 32452 | 2046.6 | 40672 | 2185.1 | 32440 | 3695.6 | 33676 | >1182.4 | 32549 | 2340.9 |
| DWT 2680 | 86068 | >5589.2 | 112866 | >6928.0 | 109228 | 11967.7 | 143576 | $>3395.7$ | 85048 | $>6474.1$ |

Table 13: SAPR Results For HBTF \#7 With Several Annealing Schedules (continued)

| Column | Description |
| :--- | :--- |
| Matrix Name | Harwell-Boeing designation of the matrix |
| Profile | SAPR profile resulting from annealing schedule S1-S5 <br> described in Table 3 (best results boxed) |
| Time | total (user + system) CPU time (sec) required on a <br> Sun SPARCstation-2 4/690 to perform the corresponding SAPR |
| $>$ | flags certain SA profile computations that did not converge <br> after the temperature fell below 0.01 (all profile changes <br> affect overall results) |

Table 14: Key to Tables 12-13

| Matrix | Conventional Profiles |  |  |  | Current |  |  | Previous <br> SAPR <br> Profile | $f_{\text {Arm }}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | RCM |  |  | GK |  |  |  |  |  |
| Name | Cav | Eve | Cur |  | Profile | Time | $f_{\text {SAPR }}$ |  |  |
| DWT 59 | 255 | 313 | 255 | 255 | 214 | 19.6 | 0.839 | 273 | 0.784 |
| DWT 66 | 151 | 211 | 151 | 127 | 127 | 24.4 | 1.000 | 193 | 0.658 |
| DWT 72 | 297 | 245 | 297 | 255 | 147 | 17.8 | 0.600 | 219 | 0.671 |
| DWT 87 | 609 | 687 | 575 | 595 | 428 | 50.4 | 0.744 | 515 | 0.831 |
| DWT 162 | 1479 | 1604 | 1456 | 1417 | 1110 | 131.4 | 0.783 | 1272 | 0.873 |
| DWT 193 | 5312 | 4844 | 4948 | 4416 | 4217 | 543.0 | 0.955 | 4409 | 0.956 |
| DWT 198 | 1219 | 1366 | 1186 | 1115 | 1090 | 158.1 | 0.978 | 1287 | 0.847 |
| DWT 209 | 3610 | 3950 | 3568 | 3823 | 2493 | 199.9 | 0.699 | 2693 | 0.926 |
| DWT 221 | 2004 | 2166 | 2147 | 2002 | 1634 | 364.9 | 0.816 | 1848 | 0.884 |
| DWT 234 | 1305 | 1544 | 1366 | 1115 | 814 | 95.3 | 0.730 | 1016 | 0.801 |
| DWT 245 | 5196 | 4018 | 5155 | 3568 | 1939 | 153.9 | 0.543 | 2161 | 0.897 |
| DWT 307 | 8336 | 8136 | 8730 | 8540 | 6290 | 304.5 | 0.773 | 6535 | 0.963 |
| DWT 310 | 2836 | 3007 | 2789 | 2697 | 2631 | 603.5 | 0.976 | 2940 | 0.895 |
| DWT 346 | 7688 | 7508 | 7714 | 7335 | 5842 | 446.2 | 0.796 | 6136 | 0.952 |
| DWT 361 | 4714 | 5090 | 4714 | 4699 | 4638 | 194.9 | 0.987 | 4992 | 0.929 |
| DWT 419 | 8230 | 9050 | 8246 | 7654 | 6147 | 1034.5 | 0.803 | 6512 | 0.944 |
| DWT 492 | 6575 | 6691 | 6982 | 5021 | 2855 | 902.4 | 0.569 | 3304 | 0.864 |
| DWT 503 | 14816 | 15945 | 14829 | 14539 | 11599 | 1079.6 | 0.798 | 11958 | 0.970 |
| DWT 512 | 4807 | 5325 | 4740 | 4456 | 3918 | 438.5 | 0.879 | 4384 | 0.894 |
| DWT 592 | 10848 | 14563 | 11207 | 10333 | 8914 | 805.6 | 0.863 | 9417 | 0.947 |

Table 15: Comparison of SAPR With Conventional and Previous SA Profile Reduction Results

| Matrix <br> Name | Conventional Profiles |  |  |  | Current |  | $f_{\text {SAPR }}$ | Previous <br> SAPR <br> Profile | $f_{\text {Arm }}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | RCM |  |  | GK | SAPR |  |  |  |  |
|  | Cav | Eve | Cur |  | Profile | Time |  |  |  |
| DWT 607 | 17261 | 15721 | 17151 | 14283 | 12613 | 1428.6 | 0.883 | 13065 | 0.965 |
| DWT 758 | 7822 | 11370 | 7808 | 7417 | 7111 | 1409.6 | 0.959 | 7123 | 0.998 |
| DWT 869 | 18424 | 16163 | 15660 | 14589 | 11723 | 701.8 | 0.804 | 13207 | 0.888 |
| DWT 878 | 21513 | 20545 | 21485 | 18818 | 17499 | 1472.7 | 0.930 | 17835 | 0.981 |
| DWT 918 | 22187 | 22399 | 22201 | 19580 | 15286 | 1394.2 | 0.781 | 15949 | 0.958 |
| DWT 992 |  | 35018 | 37136 |  | 31940 | 7637.3 | 0.912 | 32528 | 0.982 |
| DWT 1005 |  | 41104 | 42176 |  | 32167 | 2816.1 | 0.783 | 32513 | 0.989 |
| DWT 1007 |  | 24168 | 23685 |  | 16965 | 2805.7 | 0.716 | 19913 | 0.852 |
| DWT 1242 |  | 51419 | 48837 |  | 32440 | 3695.6 | 0.664 | 33098 | 0.980 |
| DWT 2680 |  | 105324 | 102112 |  | 85048 | 6474.1 | 0.833 | 84900 | 1.002 |

Table 16: Comparison of SAPR With Conventional and Previous SA Profile Reduction Results (continued)

| Column | Description |
| :--- | :--- |
| Matrix Name | Harwell-Boeing designation of the matrix |
| Conventional Profiles | non-SA profiles from various sources <br> (best results boxed) |
| Cav | Reverse Cuthill-McKee profile derived from <br> SPARSPAK library (source: [3]) |
| Eve | RCM profile (source: [5]) |
| Cur | RCM profile computed by author using pseudoperipheral |
| GK algorithm described in [6] |  |

Table 17: Key to Tables 15-16

| $\begin{gathered} \mathrm{H}-\mathrm{B} \\ \# \end{gathered}$ | Matrix | $N$ | \# of <br> Matrix <br> Nonzeros | Conventional |  |  | Simulated <br> Annealing |  | $f_{S A F R}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  | Fills |  |  |  |  |
|  | Name |  |  | ND | MDA | CTB | Fill | Time |  |
| 3 | ASH85 | 85 | 304 | 390 | 211 |  | 195 | 6122.9 | 0.924 |
| 4 | BCSPWR01 | 39 | 85 | 23 | 19 |  | 19 | 118.4 | 1.000 |
|  | BCSPWR02 | 49 | 108 | 49 | 21 |  | 20 | 206.2 | 0.952 |
| 5 | BCSSTK01 | 48 | 224 | 336 | 269 |  | 231 | 5849.2 | 0.859 |
| 6 | CAN 24 | 24 | 92 | 34 | 27 |  | 23 | 179.6 | 0.852 |
|  | CAN 61 | 61 | 309 | 112 | 56 |  | 52 | 2699.9 | 0.929 |
|  | CAN 62 | 62 | 140 | 97 | 44 |  | 44 | 430.2 | 1.000 |
|  | CAN 73 | 73 | 225 | 263 | 163 |  | 164 | 4901.6 | 1.006 |
|  | CAN 96 | 96 | 432 | 699 | 544 |  | 545 | 40062.6 | 1.002 |
| 7 | DWT 59 | 59 | 163 | 121 | 81 |  | 79 | 771.8 | 0.975 |
|  | DWT 66 | 66 | 193 | 110 | 0 |  | 8 | 554.8 | ERROR |
|  | DWT 72 | 72 | 147 | 87 | 37 |  | 37 | 351.0 | 1.000 |
|  | DWT 87 | 87 | 314 | 319 | 105 |  | 99 | 4388.6 | 0.943 |
| 28 | 685 BUS | 685 | 1967 | 4212 | 1692 | 1586 | 1523 | 20700.0 | 0.960 |
|  | 1138 BUS | 1138 | 2596 | 3838 | 673 | 641 | 691 | 22900.0 | 1.078 |

Table 18: SAFR Results

| Column | Description |
| :--- | :--- |
| H-B \# | Harwell-Boeing "Tape File Number" |
| Matrix Name | Harwell-Boeing designation of the matrix |
| $N$ | dimension of the matrix is $N \times N$ |
| \# of Matrix Nonzeros | number of non-zero elements in the matrix |
| Conventional Fills | non-SA fills from various sources |
| ND | best results boxed) fill from conventional nested dissection |
| MDA | ordering (source: [7]) |
| best fill resulting from conventional minimum-degree |  |
| CTB | best fill resulting from minimum-degree algorithm ordering (source: [7]) |
| Fill | with the tie-breaking strategy in [2] |
| Sime SPARCstation-2 to perform SAFR |  |
| total (user + system) CPU time (sec) required on a |  |
| batio of Fill to the minimum of ND, MDA, and CTB |  |

Table 19: Key to Table 18
$8 \quad$ Figures


Figure 1:


Figure 2:


Figure 3:


Figure 4:


Figure 5:


Figure 6:


Figure 7:


Figure 8:


Figure 9:


Figure 10:


Figure 11:


Figure 12:


Figure 13 :


Figure 14:

## LEGENDS

Figure 1: Swapping Two Rows And Columns of a Symmetric Matrix

Figure 2: A Simple Example

Figure 3: Sparsity Pattern of Original Figure 2 Matrix

Figure 4: Sparsity Pattern of RCM-ordered Figure 2 Matrix

Figure 5: Sparsity Pattern of SA Profile Reduction of Figure 2 Matrix

Figure 6: Sparsity Pattern of Original $100 \times 100$ 2D 5-point PDE Matrix

Figure 7: Sparsity Pattern of RCM-ordered $100 \times 100$ 2D 5-point PDE Matrix

Figure 8: Sparsity Pattern of SA Profile Reduction of $100 \times 100$ 2-D 5-point PDE Matrix

Figure 9: $f_{S A P R}$ vs. $N$ for a Range of 2-D 5-point PDE Matrices

Figure 10: Relative Performance of SAPR vs. $N$

Figure 11: Relative Performance of SAPR vs. Harwell-Boeing Tape File Number

Figure 12: Sparsity Pattern of SAFR of Figure 2 Matrix

Figure 13: Sparsity Pattern of SAFR of $100 \times 100$ 2-D 5-point PDE Matrix

Figure 14: Times Required for SA Fill and Profile Minimization of 2-D 5-point PDE Matrix


[^0]:    ${ }^{1}$ The timings for Tables 6-10 and those for S1 in Tables 12-13 differ as the former were taken from an earlier, less efficient version of the software with a different compiler and operating system on a different SPARCstation- 2 .

[^1]:    ${ }^{2}$ If we consider over 5 CPU-hours to be "reasonable"!

