

Black-Box Optimization Benchmarking Template for Noiseless Function Testbed

Draft version *

Forename Name

ABSTRACT

Categories and Subject Descriptors

G.1.6 [Numerical Analysis]: Optimization—*global optimization, unconstrained optimization*; F.2.1 [Analysis of Algorithms and Problem Complexity]: Numerical Algorithms and Problems

General Terms

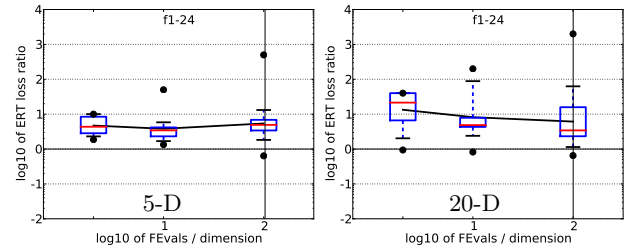
Algorithms

Keywords

Benchmarking, Black-box optimization

1. RESULTS

Results of CMA-ES from experiments according to [?] on the benchmark functions given in [?, ?] are presented in Figures ??, ?? and ?? and in Tables ?? and ??.



<i>f1-f24 in 5-D, maxFE/D=103</i>						
#FEs/D	best	10%	25%	med	75%	90%
2	1.9	2.3	2.7	4.4	8.5	10
10	1.3	1.6	2.3	3.4	4.2	10
100	0.64	1.6	3.1	4.9	7.0	18
1e3	0.66	2.0	4.8	17	29	96
RL _{US} /D	1e2	1e2	1e2	1e2	1e2	1e2
<i>f1-f24 in 20-D, maxFE/D=100</i>						
#FEs/D	best	10%	25%	med	75%	90%
2	0.94	1.9	6.4	21	40	40
10	0.82	2.2	4.3	4.9	8.3	1.1e2
100	0.65	1.1	2.3	3.4	16	70
1e3	1.1	2.7	4.4	11	35	4.8e2
RL _{US} /D	1e2	1e2	1e2	1e2	1e2	1e2

Figure 3: ERT loss ratio versus the budget (both in number of f -evaluations divided by dimension). The target value f_t for a given budget FEvals is the best target f -value reached within the budget by the given algorithm. Shown is the ERT of the given algorithm divided by best ERT seen in GECCO-BBOB-2009 for the target f_t , or, if the best algorithm reached a better target within the budget, the budget divided by the best ERT. Line: geometric mean. Box-Whisker error bar: 25-75%-ile with median (box), 10-90%-ile (caps), and minimum and maximum ERT loss ratio (points). The vertical line gives the maximal number of function evaluations in a single trial in this function subset. See also Figure ?? for results on each function subgroup.

*Submission deadline: March 28th.

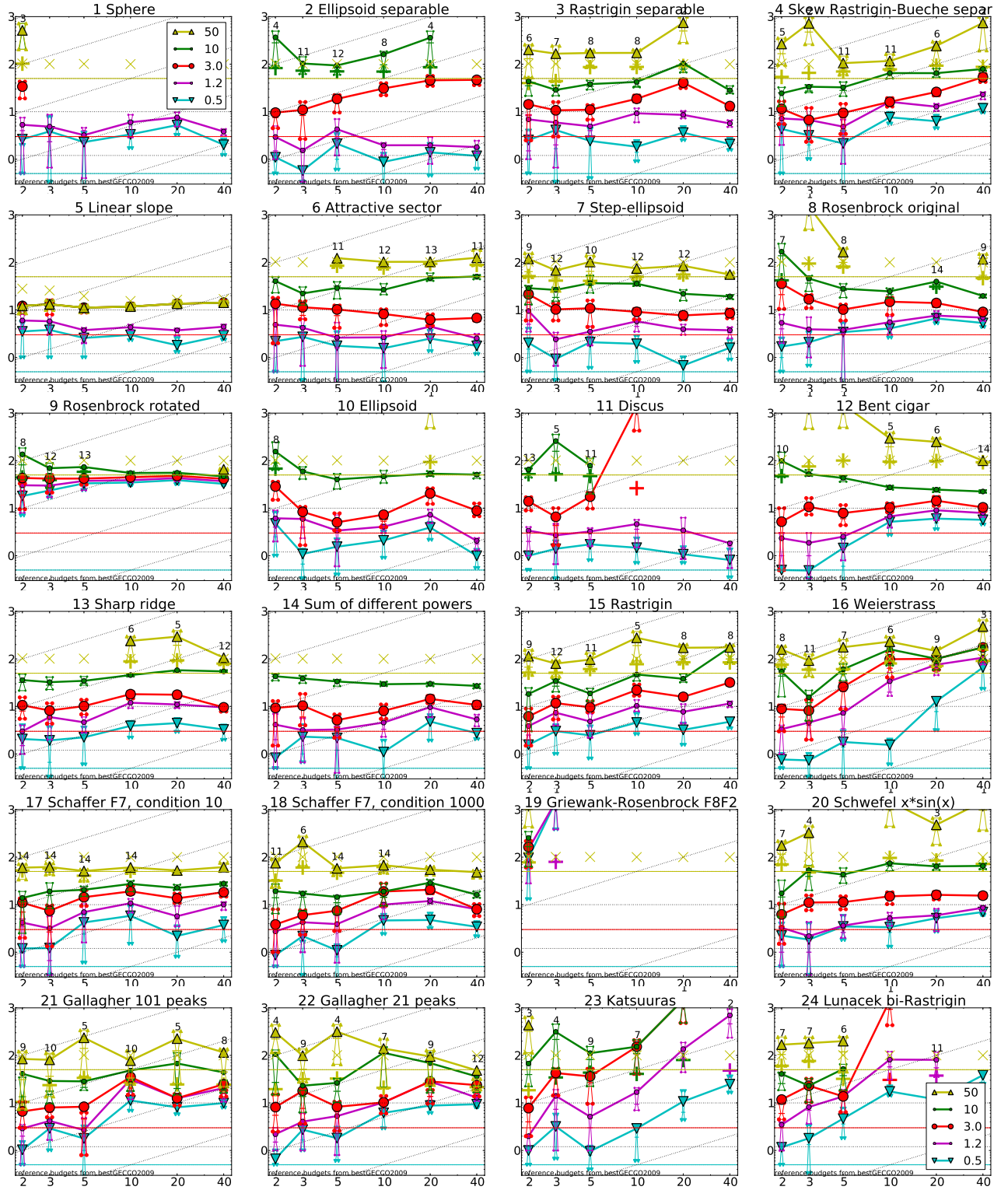


Figure 1: Expected number of f -evaluations (ERT, lines) to reach $f_{\text{opt}} + \Delta f$; median number of f -evaluations (+) to reach the most difficult target that was reached not always but at least once; maximum number of f -evaluations in any trial (x); interquartile range with median (notched boxes) of simulated runlengths to reach $f_{\text{opt}} + \Delta f$; all values are divided by dimension and plotted as \log_{10} values versus dimension. Shown is the ERT for targets just not reached by the GECCO-BBOB-2009 best algorithm within the given budget $k\text{DIM}$, where k is shown in the legend. Numbers above ERT-symbols indicate the number of trials reaching the respective target. Slanted grid lines indicate a scaling with $\mathcal{O}(\text{DIM})$ compared to $\mathcal{O}(1)$ when using the respective 2009 best algorithm.

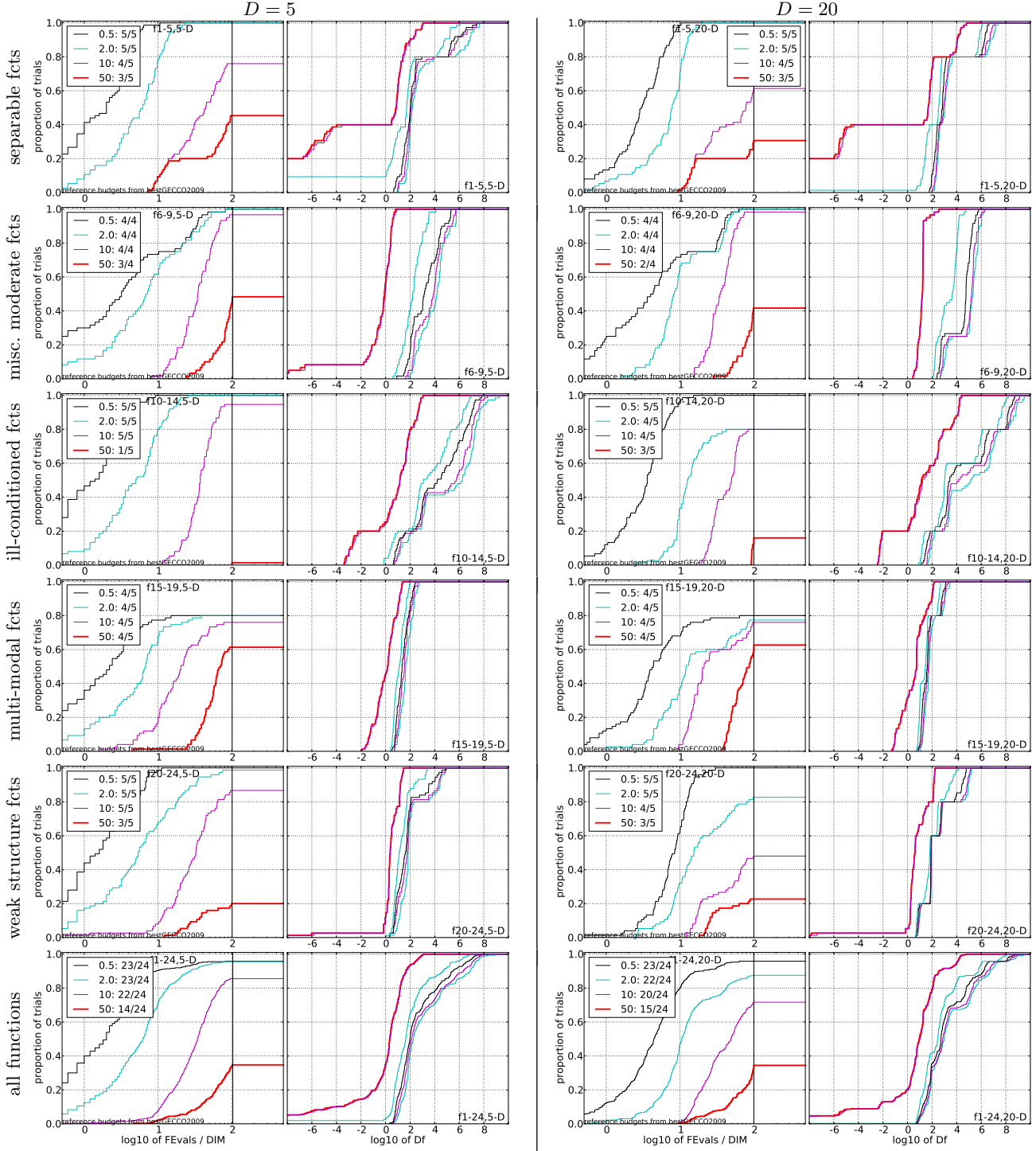


Figure 2: Empirical cumulative distribution functions (ECDF), plotting the fraction of trials with an outcome not larger than the respective value on the x -axis. Left subplots: ECDF of number of function evaluations (FEvals) divided by search space dimension D , to fall below $f_{\text{opt}} + \Delta f$ where Δf is the target just not reached by the GECCO-BBOB-2009 best algorithm within a budget of $k \times \text{DIM}$ evaluations, where k is the first value in the legend. Legends indicate for each target the number of functions that were solved in at least one trial within the displayed budget. Right subplots: ECDF of the best achieved Δf for running times of $0.5D, 1.2D, 3D, 10D, 100D, 1000D, \dots$ function evaluations (from right to left cycling cyan-magenta-black...) and final Δf -value (red), where Δf and Df denote the difference to the optimal function value.

#FEs/D	5-D					#succ
	0.5	1.2	3.0	10	50	
f₁	<i>2.5e+1:4.8</i>	<i>1.6e+1:7.6</i>	<i>1.0e-8:12</i>	<i>1.0e-8:12</i>	<i>1.0e-8:12</i>	15/15
	2.4(2)	2.1(2)	∞	∞	∞510	0/15
f₂	<i>1.6e+6:2.9</i>	<i>4.0e+5:11</i>	<i>4.0e+4:15</i>	<i>6.3e+2:58</i>	<i>1.0e-8:95</i>	15/15
	3.7(5)	1.9(2)	6.1(3)	8.2(5)	∞510	0/15
f₃	<i>1.6e+2:4.1</i>	<i>1.0e+2:15</i>	<i>6.3e+1:23</i>	<i>2.5e+1:73</i>	<i>1.0e+1:716</i>	15/15
	2.9(3)	1.7(1)	2.3(2)	2.6(1)	1.2(1)	8/15
f₄	<i>2.5e+2:2.6</i>	<i>1.6e+2:10</i>	<i>1.0e+2:19</i>	<i>4.0e+1:65</i>	<i>1.6e+1:434</i>	15/15
	4.1(4)	2.5(4)	2.5(3)	2.5(1)	1.2(0.8)	11/15
f₅	<i>6.3e+1:4.0</i>	<i>4.0e+1:10</i>	<i>1.0e-8:10</i>	<i>1.0e-8:10</i>	<i>1.0e-8:10</i>	15/15
	3.2(2)	1.9(2)	5.6(1)	5.6(1)	5.6(1)	15/15
f₆	<i>1.0e+5:3.0</i>	<i>2.5e+4:8.4</i>	<i>1.0e+2:16</i>	<i>2.5e+1:54</i>	<i>2.5e-1:254</i>	15/15
	2.9(4)	1.6(2)	3.2(4)	2.7(2)	2.4(1)	11/15
f₇	<i>1.6e+2:4.2</i>	<i>1.0e+2:6.2</i>	<i>2.5e+1:20</i>	<i>4.0e+0:54</i>	<i>1.0e+0:324</i>	15/15
	2.5(3)	2.8(3)	2.7(2)	3.4(2)	1.6(2)	10/15
f₈	<i>1.0e+4:4.6</i>	<i>6.3e+3:6.8</i>	<i>1.0e+3:18</i>	<i>6.3e+1:54</i>	<i>1.6e+0:258</i>	15/15
	3.7(3)	2.8(3)	2.9(2)	2.6(1)	3.2(3)	8/15
f₉	<i>2.5e+1:20</i>	<i>1.6e+1:26</i>	<i>1.0e+1:35</i>	<i>4.0e+0:62</i>	<i>1.6e-2:256</i>	15/15
	8.4(3)	7.3(3)	6.1(3)	6.0(5)	∞510	0/15
f₁₀	<i>2.5e+6:2.9</i>	<i>6.3e+5:7.0</i>	<i>2.5e+5:17</i>	<i>6.3e+3:54</i>	<i>2.5e+1:297</i>	15/15
	2.7(3)	2.4(3)	1.5(1)	3.8(2)	∞510	0/15
f₁₁	<i>1.0e+6:3.0</i>	<i>6.3e+4:6.2</i>	<i>6.3e+2:16</i>	<i>6.3e+1:74</i>	<i>6.3e-1:298</i>	15/15
	2.9(2)	2.6(3)	5.5(5)	5.3(5)	∞510	0/15
f₁₂	<i>4.0e+7:3.6</i>	<i>1.6e+7:7.6</i>	<i>4.0e+6:19</i>	<i>1.6e+4:52</i>	<i>1.0e+0:268</i>	15/15
	2.0(3)	1.7(2)	2.1(2)	4.2(1)	28(30)	1/15
f₁₃	<i>1.0e+3:2.8</i>	<i>6.3e+2:8.4</i>	<i>4.0e+2:17</i>	<i>6.3e+1:52</i>	<i>6.3e-2:264</i>	15/15
	4.0(4)	2.8(2)	3.0(2)	3.3(1.0)	∞510	0/15
f₁₄	<i>1.6e+1:3.0</i>	<i>1.0e+1:10</i>	<i>6.3e+0:15</i>	<i>2.5e-1:53</i>	<i>1.0e-5:251</i>	15/15
	3.6(6)	1.7(2)	1.7(2)	3.2(1)	∞510	0/15
f₁₅	<i>1.6e+2:3.0</i>	<i>1.0e+2:13</i>	<i>6.3e+1:24</i>	<i>4.0e+1:55</i>	<i>1.6e+1:289</i>	5/5
	4.1(4)	1.9(2)	2.0(0.9)	1.7(0.9)	1.7(1)	11/15
f₁₆	<i>4.0e+1:4.8</i>	<i>2.5e+1:16</i>	<i>1.6e+1:46</i>	<i>1.0e+1:120</i>	<i>4.0e+0:334</i>	15/15
	1.9(2)	2.3(4)	2.8(2)	2.5(3)	2.6(2)	7/15
f₁₇	<i>1.0e+1:5.2</i>	<i>6.3e+0:26</i>	<i>4.0e+0:57</i>	<i>2.5e+0:110</i>	<i>6.3e-1:412</i>	15/15
	4.1(6)	1.3(1)	1.3(1.0)	0.93(0.4)	0.62(0.3) ↓	14/15
f₁₈	<i>6.3e+1:3.4</i>	<i>4.0e+1:7.2</i>	<i>2.5e+1:20</i>	<i>1.6e+1:58</i>	<i>1.6e+0:318</i>	15/15
	1.6(2)	2.7(3)	1.9(1)	1.2(0.7)	0.92(0.3)	14/15
f₁₉	<i>1.6e-1:172</i>	<i>1.0e-1:242</i>	<i>6.3e-2:675</i>	<i>4.0e-2:3078</i>	<i>2.5e-2:4946</i>	15/15
	∞	∞	∞	∞	∞510	0/15
f₂₀	<i>6.3e+3:5.1</i>	<i>4.0e+3:8.4</i>	<i>4.0e+1:15</i>	<i>2.5e+0:69</i>	<i>1.0e+0:851</i>	15/15
	3.4(3)	2.2(2)	3.7(2)	3.1(1)	∞510	0/15
f₂₁	<i>4.0e+1:3.9</i>	<i>2.5e+1:11</i>	<i>1.6e+1:31</i>	<i>6.3e+0:73</i>	<i>1.6e+0:347</i>	5/5
	2.3(3)	1.3(1)	1.3(2)	2.0(1)	3.4(4)	5/15
f₂₂	<i>6.3e+1:3.6</i>	<i>4.0e+1:15</i>	<i>2.5e+1:32</i>	<i>1.0e+1:71</i>	<i>1.6e+0:341</i>	5/5
	2.5(3)	1.8(2)	1.3(2)	1.9(1)	4.6(5)	4/15
f₂₃	<i>1.0e+1:3.0</i>	<i>6.3e+0:9.0</i>	<i>4.0e+0:33</i>	<i>2.5e+0:84</i>	<i>1.0e+0:518</i>	15/15
	1.6(1)	2.9(3)	5.4(5)	6.7(7)	∞510	0/15
f₂₄	<i>6.3e+1:15</i>	<i>4.0e+1:37</i>	<i>4.0e+1:37</i>	<i>2.5e+1:118</i>	<i>1.6e+1:692</i>	15/15
	1.6(2)	1.9(2)	1.9(2)	2.2(2)	1.4(1)	6/15

#FEs/D	20-D					#succ
	0.5	1.2	3.0	10	50	
f₁	<i>6.3e+1:24</i>	<i>4.0e+1:42</i>	<i>1.0e-8:43</i>	<i>1.0e-8:43</i>	<i>1.0e-8:43</i>	15/15
	4.3(2)	3.6(2)	∞	∞	∞2000	0/15
f₂	<i>4.0e+6:29</i>	<i>2.5e+6:42</i>	<i>1.0e+5:65</i>	<i>1.0e+4:207</i>	<i>1.0e-8:412</i>	15/15
	0.97(0.9)	0.94(0.7)	14(5)	35(32)	∞2000	0/15
f₃	<i>6.3e+2:33</i>	<i>4.0e+2:44</i>	<i>1.6e+2:109</i>	<i>1.0e+2:255</i>	<i>2.5e+1:3277</i>	15/15
	2.2(1)	3.9(2)	7.5(3)	8.1(4)	4.5(5)	2/15
f₄	<i>6.3e+2:22</i>	<i>4.0e+2:91</i>	<i>2.5e+2:250</i>	<i>1.6e+2:332</i>	<i>6.3e+1:1927</i>	15/15
	5.8(3)	2.8(1)	2.1(0.7)	3.9(1)	2.5(2)	6/15
f₅	<i>2.5e+2:19</i>	<i>1.6e+2:34</i>	<i>1.0e-8:41</i>	<i>1.0e-8:41</i>	<i>1.0e-8:41</i>	15/15
	1.9(1)	2.2(0.7)	6.7(1)	6.7(1)	6.7(1)	15/15
f₆	<i>2.5e+5:16</i>	<i>6.3e+4:43</i>	<i>1.6e+4:62</i>	<i>1.6e+2:353</i>	<i>1.6e+1:1078</i>	15/15
	3.1(2)	2.1(0.9)	2.0(0.9)	2.6(1)	1.9(1)	13/15
f₇	<i>1.0e+3:11</i>	<i>4.0e+2:39</i>	<i>2.5e+2:74</i>	<i>6.3e+1:319</i>	<i>1.0e+1:1351</i>	15/15
	1.3(1)	2.0(1)	2.1(0.8)	1.4(0.4)	1.3(0.9)	12/15
f₈	<i>4.0e+4:19</i>	<i>2.5e+4:35</i>	<i>4.0e+3:67</i>	<i>2.5e+2:231</i>	<i>1.6e+1:1470</i>	15/15
	7.0(4)	4.3(2)	4.2(0.8)	3.4(2)	∞2000	0/15
f₉	<i>1.0e+2:357</i>	<i>6.3e+1:560</i>	<i>4.0e+1:684</i>	<i>2.5e+1:756</i>	<i>1.0e+1:1716</i>	15/15
	2.2(0.5)	1.5(0.3)	1.4(0.2)	1.5(0.3)	∞2000	0/15
f₁₀	<i>1.6e+6:15</i>	<i>1.0e+6:27</i>	<i>4.0e+5:70</i>	<i>6.3e+4:231</i>	<i>4.0e+3:1015</i>	15/15
	5.2(4)	5.3(3)	5.8(4)	4.6(1)	30(34)	1/15
f₁₁	<i>4.0e+4:11</i>	<i>2.5e+3:27</i>	<i>1.6e+2:313</i>	<i>1.0e+2:481</i>	<i>1.0e+1:1002</i>	15/15
	1.9(1)	2.5(2)	∞	∞	∞2000	0/15
f₁₂	<i>1.0e+8:23</i>	<i>6.3e+7:39</i>	<i>2.5e+7:76</i>	<i>4.0e+6:209</i>	<i>1.0e+1:1042</i>	15/15
	5.2(3)	4.6(2)	3.8(1)	2.4(0.4)	4.8(4)	6/15
f₁₃	<i>1.6e+3:28</i>	<i>1.0e+3:64</i>	<i>6.3e+2:79</i>	<i>4.0e+1:211</i>	<i>2.5e+0:1724</i>	15/15
	3.2(2)	3.4(1)	4.5(0.9)	5.5(0.5)	3.4(3)	5/15
f₁₄	<i>2.5e+1:15</i>	<i>1.6e+1:42</i>	<i>1.0e+1:75</i>	<i>1.6e+0:219</i>	<i>6.3e-4:1106</i>	15/15
	6.6(4)	4.6(3)	3.8(1)	2.8(0.6)	∞2000	0/15
f₁₅	<i>6.3e+2:15</i>	<i>4.0e+2:67</i>	<i>2.5e+2:292</i>	<i>1.6e+2:846</i>	<i>1.0e+2:1671</i>	15/15
	4.2(4)	2.3(1)	1.1(0.2)	0.90(0.3)	2.1(1)	8/15
f₁₆	<i>4.0e+1:26</i>	<i>2.5e+1:127</i>	<i>1.6e+1:540</i>	<i>1.6e+1:540</i>	<i>1.0e+1:1384</i>	15/15
	10(9)	12(8)	3.7(3)	3.7(3)	2.1(2)	9/15
f₁₇	<i>1.6e+1:11</i>	<i>1.0e+1:63</i>	<i>6.3e+0:305</i>	<i>4.0e+0:468</i>	<i>1.0e+0:1030</i>	15/15
	4.2(4)	1.8(1)	0.89(0.3)	0.96(0.3)	1.0(0.5)	15/15
f₁₈	<i>4.0e+1:116</i>	<i>2.5e+1:252</i>	<i>1.6e+1:430</i>	<i>1.0e+1:621</i>	<i>4.0e+0:1090</i>	15/15
	0.82(0.8)	0.95(0.4)	0.96(0.3)	0.94(0.3)	1.0(0.3)	15/15
f₁₉	<i>1.6e-1:2.5e5</i>	<i>1.0e-1:3.4e5</i>	<i>6.3e-2:3.4e5</i>	<i>4.0e-2:3.4e5</i>	<i>2.5e-2:3.4e5</i>	3/15
	∞	∞	∞	∞	∞2000	0/15
f₂₀	<i>1.6e+4:38</i>	<i>1.0e+4:42</i>	<i>2.5e+2:62</i>	<i>2.5e+0:250</i>	<i>1.6e+0:2536</i>	15/15
	2.7(1)	2.8(2)	5.2(1)	5.1(1)	3.8(4)	3/15
f₂₁	<i>6.3e+1:36</i>	<i>4.0e+1:77</i>	<i>4.0e+1:77</i>	<i>1.6e+1:456</i>	<i>4.0e+0:1094</i>	15/15
	4.5(2)	3.3(1)	3.3(1)	3.0(4)	4.1(5)	5/15
f₂₂	<i>6.3e+1:45</i>	<i>4.0e+1:68</i>	<i>4.0e+1:68</i>	<i>1.6e+1:231</i>	<i>6.3e+0:1219</i>	15/15
	3.9(2)	8.4(15)	8.4(15)	6.0(9)	1.6(2)	9/15
f₂₃	<i>6.3e+0:29</i>	<i>4.0e+0:118</i>	<i>2.5e+0:306</i>	<i>2.5e+0:306</i>	<i>1.0e+0:1614</i>	15/15
	7.5(8)	23(25)	97(105)	97(105)	∞2000	0/15
f₂₄	<i>2.5e+2:208</i>	<i>1.6e+2:918</i>	<i>1.0e+2:6628</i>	<i>6.3e+1:9885</i>	<i>4.0e+1:31629</i>	15/15
	1.1(0.3)	1.8(1)	∞	∞	∞2000	0/15

Table 1: Expected running time (ERT in number of function evaluations) divided by the best ERT measured during BBOB-2009. The ERT and in braces, as dispersion measure, the half difference between 90 and 10%-tile of bootstrapped run lengths appear in the second row of each cell, the best ERT (preceded by the target Δf -value in *italics*) in the first. #succ is the number of trials that reached the target value of the last column. The median number of conducted function evaluations is additionally given in *italics*, if the target in the last column was never reached. Bold entries are statistically significantly better (according to the rank-sum test) compared to the best algorithm in BBOB-2009, with $p = 0.05$ or $p = 10^{-k}$ when the number $k > 1$ is following the ↓ symbol, with Bonferroni correction by the number of functions.

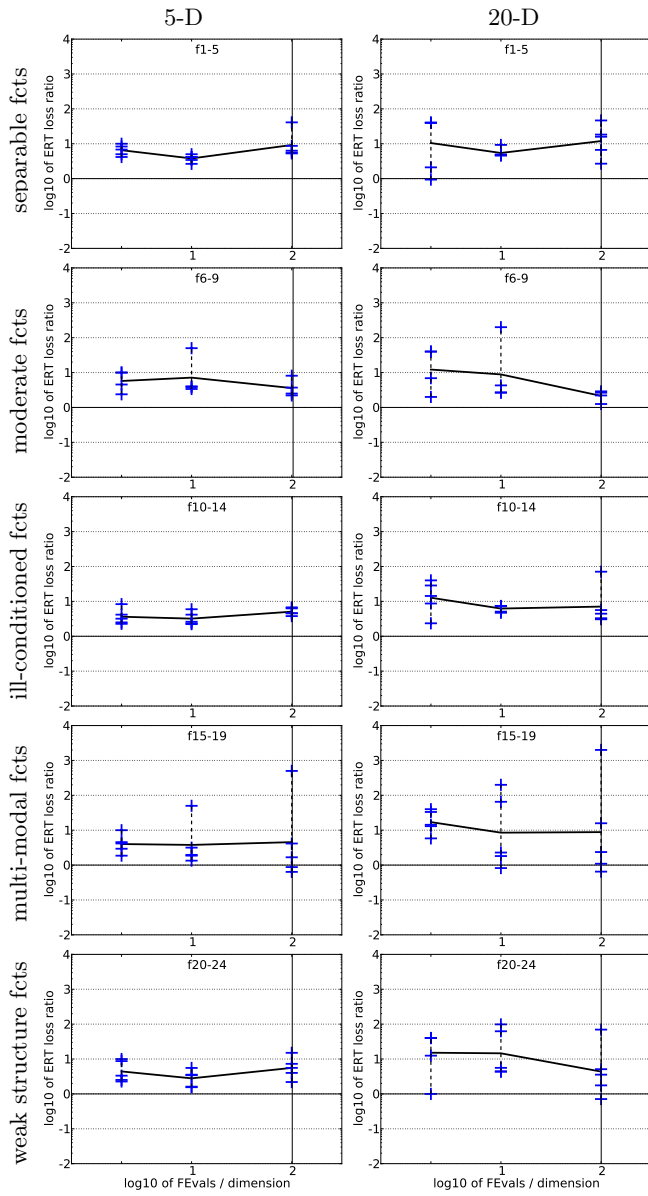


Figure 4: ERT loss ratios (see Figure ?? for details). Each cross (+) represents a single function, the line is the geometric mean.