

### **Shallow water equations**

• To recap, using eta for depth=h+H:  $\frac{D\eta}{Dt} = -\eta \nabla \cdot u$ 

$$\frac{Du}{Dt} = -g\nabla h$$

 We're currently working on the advection (material derivative) part

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### **Exploiting Lagrangian view**

- We want to stick an Eulerian grid for now, but somehow exploit the fact that
  - If we know q at some point x at time t, we just follow a particle through the flow starting at x to see where that value of q ends up

$$q(x(t + \Delta t), t + \Delta t) = q(x(t), t)$$
$$\frac{dx}{dt} = u(x), \quad x(t) = x_0$$

### Looking backwards

- Problem with tracing particles we want values at grid nodes at the end of the step
  - Particles could end up anywhere
- But... we can look backwards in time

$$q_{ijk} = q(x(t - \Delta t), t - \Delta t)$$
$$\frac{dx}{dt} = u(x), \quad x(t) = x_{ijk}$$

- Same formulas as before but new interpretation
  - To get value of q at a grid point, follow a particle backwards through flow to wherever it started

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### Semi-Lagrangian method

- Developed in weather prediction, going back to the 50's
- Also dubbed "stable fluids" in graphics (reinvention by Stam '99)
- To find new value of q at a grid point, trace particle backwards from grid point (with velocity u) for -∆t and interpolate from old values of q
- Two questions
  - How do we trace?
  - How do we interpolate?

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# <section-header> Fracing Tracing backwards aren't too big a deal We don't compound them - stability isn't an issue How accurate we are in tracing doesn't effect shape of q much, just location Whether we get too much blurring, oscillations, or a nice result is really up to interpolation Thus look at "Forward" Euler and RK2

### **Tracing: 1st order**

- We're at grid node (i,j,k) at position x<sub>ijk</sub>
- Trace backwards through flow for -Δt

$$x_{old} = x_{ijk} - \Delta t \, u_{ijk}$$

- Note using u value at grid point (what we know already) like Forward Euler.
- Then can get new q value (with interpolation)

$$q_{ijk}^{n+1} = q^n (x_{old})$$
$$= q^n (x_{ijk} - \Delta t u_{ijk})$$

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### Interpolation

- "First" order accurate: nearest neighbour
  - Just pick q value at grid node closest to x<sub>old</sub>
  - Doesn't work for slow fluid (small time steps) -- nothing changes!
  - When we divide by grid spacing to put in terms of advection equation, drops to zero'th order accuracy
- "Second" order accurate: linear or bilinear (2D)
  - Ends up first order in advection equation
  - Still fast, easy to handle boundary conditions...
  - How well does it work?

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### Linear interpolation

• Error in linear interpolation is proportional to  $\sum_{i=1}^{n}$ 

 $\Delta x^2 \frac{\partial^2 q}{\partial x^2}$ 

Modified PDE ends up something like...

$$\frac{Dq}{Dt} = k(\Delta t)\Delta x^2 \frac{\partial^2 q}{\partial x^2}$$

- We have numerical viscosity, things will smear out
- For reasonable time steps, k looks like  $1/\Delta t \sim 1/\Delta x$
- [Equivalent to 1st order upwind for CFL Δt]
- In practice, too much smearing for inviscid fluids

cs533d-term1-2005 10

## Nice properties of lerping

- Linear interpolation is completely stable
  - Interpolated value of q must lie between the old values of q on the grid
  - Thus with each time step, max(q) cannot increase, and min(q) cannot decrease
- Thus we end up with a fully stable algorithm - take Δt as big as you want
  - Great for interactive applications
  - Also simplifies whole issue of picking time steps

### **Cubic interpolation**

- To fix the problem of excessive smearing, go to higher order
- ◆ E.g. use cubic splines
  - Finding interpolating C<sup>2</sup> cubic spline is a little painful, an alternative is the
  - C<sup>1</sup> Catmull-Rom (cubic Hermite) spline
     [derive]
- Introduces overshoot problems
  - Stability isn't so easy to guarantee anymore

### **Min-mod limited Catmull-Rom**

- See Fedkiw, Stam, Jensen '01
- Trick is to check if either slope at the endpoints of the interval has the wrong sign
  - If so, clamp the slope to zero
  - Still use cubic Hermite formulas with more reliable slopes
- This has same stability guarantee as linear interpolation
  - But in smoother parts of flow, higher order accurate
  - Called "high resolution"
- Still has issues with boundary conditions...

cs533d-term1-2005 13

### **Back to Shallow Water**

- So we can now handle advection of both water depth and each component of water velocity
- Left with the divergence and gradient



## Staggered grid We like central differences - more accurate, unbiased So natural to use a staggered grid for velocity and height variables Called MAC grid after the Marker-and-Cell method (Harlow and Welch '65) that introduced it Heights at cell centres u-velocities at x-faces of cells w-velocities at z-faces of cells

Spatial Discretization

• So on the MAC grid:

terms

$$\frac{\partial \eta_{ij}}{\partial t} = -\eta_{ij} \left( \frac{u_{i+\frac{1}{2},j} - u_{i-\frac{1}{2},j}}{\Delta x} + \frac{w_{i,j+\frac{1}{2}} - w_{i,j-\frac{1}{2}}}{\Delta z} \right)$$
$$\frac{\partial u_{i+\frac{1}{2},j}}{\partial t} = -g \frac{h_{i+1,j} - h_{i,j}}{\Delta x}$$
$$\frac{\partial w_{i,j+\frac{1}{2}}}{\partial t} = -g \frac{h_{i,j+1} - h_{i,j}}{\Delta z}$$

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### **Solving Full Equations**

- Let's now solve the full incompressible Euler or Navier-Stokes equations
- We'll first avoid interfaces (e.g. free surfaces)
- Think smoke

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## Time integration

• Don't mix the steps at all - 1st order accurate

$$u^{(1)} = advect(u^{n}, \Delta t)$$
  

$$u^{(2)} = u^{(1)} + v\Delta t \nabla^{2} u^{(2)}$$
  

$$u^{(3)} = u^{(2)} + \Delta t g$$
  

$$u^{n+1} = u^{(3)} - \Delta t \frac{1}{2} \nabla p$$

- We've already seen how to do the advection step
- Often can ignore the second step (viscosity)
- Let's focus for now on the last step (pressure)

### **Operator Splitting**

- Generally a bad idea to treat incompressible flow as conservation laws with constraints
- Instead: split equations up into easy chunks, just like Shallow Water

$$u_{t} + u \cdot \nabla u = 0$$
  

$$u_{t} = v \nabla^{2} u$$
  

$$u_{t} = g$$
  

$$u_{t} + \frac{1}{\rho} \nabla p = 0 \qquad (\nabla \cdot u = 0)$$

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### **Advection boundary conditions**

- But first, one last issue
- Semi-Lagrangian procedure may need to interpolate from values of u outside the domain, or inside solids
  - Outside: no correct answer. Extrapolating from nearest point on domain is fine, or assuming some far-field velocity perhaps
  - Solid walls: velocity should be velocity of wall (e.g.zero)
    - Technically only normal component of velocity needs to be taken from wall, in absence of viscosity the tangential component may be better extrapolated from the fluid

19

### **Continuous pressure**

- Before we discretize in space, last step is to take u<sup>(3)</sup>, figure out the pressure p that makes u<sup>n+1</sup> incompressible:
  - Want  $\nabla \cdot u^{n+1} = 0$
  - Plug in pressure update formula:  $\nabla \cdot (u^{(3)} \Delta t \frac{1}{\rho} \nabla p) = 0$
  - Rearrange:  $\nabla \cdot (\Delta t \frac{1}{\rho} \nabla p) = \nabla \cdot u^{(3)}$
  - Solve this Poisson problem (often density is constant and you can rescale p by it, also Δt)
    - Make this assumption from now on:  $\nabla^2 n = \nabla \cdot u^{(3)}$

$$\mathbf{v} \quad p = \mathbf{v} \cdot \mathbf{u}^{(n+1)}$$
$$u^{n+1} = u^{(3)} - \nabla p$$

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21

### **Pressure boundary conditions**

- Issue of what to do for p and u at boundaries in pressure solve
- Think in terms of control volumes: subtract pn from u on boundary so that integral of u•n is zero
- So at closed boundary we end up with

$$u^{n+1} \cdot n = 0$$
$$u^{n+1} \cdot n = u^{(3)} \cdot n - \frac{\partial p}{\partial n}$$

cs533d-term1-2005 22



### **Approximate projection**

• Can now directly discretize Poisson equation on a grid  $(\nabla^2 p)_{ijk} = \left( \frac{\partial^2 p}{\partial x^2} + \frac{\partial^2 p}{\partial y^2} + \frac{\partial^2 p}{\partial z^2} \right)$   $\approx \frac{p_{i+1jk} - 2p_{ijk} + p_{i-1jk}}{\Delta x^2} + \frac{p_{ij+1k} - 2p_{ijk} + p_{ij-1k}}{\Delta y^2} + \frac{p_{ijk+1} - 2p_{ijk} + p_{ijk-1}}{\Delta z^2}$   $(\nabla \cdot u)_{ijk} = \left( \frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} + \frac{\partial w}{\partial z} \right)_{ijk}$   $\approx \frac{u_{i+1jk} - u_{i-1jk}}{2\Delta x} + \frac{v_{ij+1k} - v_{ij-1k}}{2\Delta y} + \frac{w_{ijk+1} - w_{ijk-1}}{2\Delta z}$   $(\nabla p)_{ijk} \approx \left[ \frac{p_{i+1jk} - p_{i-1jk}}{2\Delta x}, \frac{p_{ij+1k} - p_{ij-1k}}{2\Delta y}, \frac{p_{ijk+1} - p_{ijk-1}}{2\Delta z} \right]$ • Central differences - 2nd order, no bias

cs533d-term1-2005 24

### Issues

- On the plus side: simple grid, simple discretization, becomes exact in limit for smooth u...
- But it doesn't work
  - Divergence part of equation can't "see" high frequency compression waves
  - Left with high frequency oscillatory error
  - Need to filter this out smooth out velocity field before subtracting off pressure gradient
  - Filtering introduces more numerical viscosity, eliminates features on coarse grids
- Also: doesn't exactly make u incompressible
- Measuring divergence of result gives nonzero
  So let's look at exactly enforcing the incompressibility
- So let's look at exactly enforcing the incompressibility constraint

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### **Exact projection (1st try)**

- Connection
  - use the discrete divergence as a hard constraint to enforce, pressure p turns out to be the Lagrange multipliers...
- Or let's just follow the route before, but discretize divergence and gradient first
  - First try: use centred differences as before
  - u and p all "live" on same grid: u<sub>ijk</sub>, p<sub>ijk</sub>
  - This is called a "collocated" scheme

cs533d-term1-2005 26

# $\begin{array}{l} \textbf{Exact collocated projection} \\ \textbf{A} \text{ So want } & (\nabla \cdot u^{n+1})_{ijk} = 0 \\ & \frac{u_{i+1jk}^{n+1} - u_{i-1jk}^{n+1}}{2\Delta x} + \frac{v_{ij+1k}^{n+1} - v_{ij-1k}^{n+1}}{2\Delta y} + \frac{w_{ijk+1}^{n+1} - w_{ijk-1}^{n+1}}{2\Delta z} = 0 \\ \textbf{A} \text{ Update with discrete gradient of p } u^{n+1} = u^{(3)} - \nabla p \\ & u_{ijk}^{n+1} = u_{ijk}^{(3)} - \left[ \frac{p_{i+1jk} - p_{i-1jk}}{2\Delta x}, \frac{p_{ij+1k} - p_{ij-1k}}{2\Delta y}, \frac{p_{ijk+1} - p_{ijk-1}}{2\Delta z} \right] \\ \textbf{A} \text{ Plug in update formula to solve for p} \\ & \frac{p_{i+2jk} - 2p_{ijk} + p_{i-2jk}}{4\Delta x^2} + \frac{p_{ij+2k} - 2p_{ijk} + p_{ij-2k}}{4\Delta y^2} + \frac{p_{ijk+2} - 2p_{ijk} + p_{ijk-2}}{4\Delta z^2} = \\ & \frac{u_{i+1jk}^{(3)} - u_{i-1jk}^{(3)}}{2\Delta x} + \frac{v_{ij+1k}^{(3)} - v_{ij-1k}^{(3)}}{2\Delta y} + \frac{w_{ijk+1}^{(3)} - w_{ijk-1}^{(3)}}{2\Delta z} \end{array}$

Problems	
<ul> <li>Pressure problem decouples into 8 independent subproblems</li> </ul>	
<ul> <li>"Checkerboard" instability</li> </ul>	
<ul> <li>Divergence still doesn't see high-frequency compression waves</li> </ul>	
<ul> <li>Really want to avoid differences over 2 grid points, but still want centred</li> </ul>	
<ul> <li>Thus use a staggered MAC grid, as with shallow water</li> </ul>	
cs533d-term1-2005	28

### Staggered grid

- Pressure p lives in centre of cell, p<sub>ijk</sub>
- u lives in centre of x-faces,  $u_{i+1/2,j,k}$
- ♦ v in centre of y-faces, v<sub>i,j+1/2,k</sub>
- ♦ w in centre of z-faces, w<sub>i,j,k+1/2</sub>
- Whenever we need to take a difference (grad p or div u) result is where it should be
- Works beautifully with "stair-step" boundaries
  - Not so simple to generalize to other boundary geometry

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### **Exact staggered projection**

• Do it discretely as before, but now want  $(\nabla \cdot u^{n+1})_{ijk} = 0$  $\frac{u_{i+1/2jk}^{n+1} - u_{i-1/2jk}^{n+1}}{\Delta x} + \frac{v_{ij+1/2k}^{n+1} - v_{ij-1/2k}^{n+1}}{\Delta y} + \frac{w_{ijk+1/2}^{n+1} - w_{ijk-1/2}^{n+1}}{\Delta z} = 0$ • And update is $<math display="block"> u_{i+1/2jk}^{n+1} = u_{i+1/2jk}^{(3)} - \frac{p_{i+1jk} - p_{ijk}}{\Delta x}$  $v_{ij+1/2k}^{n+1} = v_{ij+1/2k}^{(3)} - \frac{p_{ij+1k} - p_{ijk}}{\Delta y}$  $w_{ijk+1/2}^{n+1} = w_{ijk+1/2}^{(3)} - \frac{p_{ijk+1} - p_{ijk}}{\Delta z}$ cs533d-term1-2005 20



### **Pressure solve simplified**

- Assume for simplicity that  $\Delta x = \Delta y = \Delta z = h$
- Then we can actually rescale pressure (again already took in density and Δt) to get

$$6p_{ijk} - p_{i+1jk} - p_{i-1jk} - p_{ij+1k} - p_{ij-1k} - p_{ijk+1} - p_{ijk+1} = -u_{i+1/2jk}^{(3)} + u_{i-1/2jk}^{(3)} - v_{ij+1/2k}^{(3)} + v_{ij-1/2k}^{(3)} - w_{ijk+1/2}^{(3)} + w_{ijk-1/2}^{(3)}$$

- At boundaries where p is known, replace (say) p<sub>i+1jk</sub> with known value, move to right-hand side (be careful to scale if not zero!)
- At boundaries where (say) ∂p/∂y=v, replace p<sub>ij+1k</sub> with p<sub>ijk</sub>+v (so finite difference for ∂p/∂y is correct at boundary)

### Solving the Linear System

- So we're left with the problem of efficiently finding p
- Luckily, linear system Ap=-d is symmetric positive definite
- Incredibly well-studied A, lots of work out there on how to do it fast

### How to solve it

- Direct Gaussian Elimination does not work well
  - This is a large sparse matrix will end up with lots of fill-in (new nonzeros)
- If domain is square with uniform boundary conditions, can use FFT
  - Fourier modes are eigenvectors of the matrix A, everything works out
- But in general, will need to go to iterative methods
  - Luckily have a great starting guess! Pressure from previous time step [appropriately rescaled]

cs533d-term1-2005 33



### **Conjugate Gradient**

- Standard iterative method for solving symmetric positive definite systems
- For a fairly exhaustive description, read
  - "An Introduction to the Conjugate Gradient Method Without the Agonizing Pain", by J. R. Shewchuk
- Basic idea: steepest descent

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### Plain vanilla CG

- ♦ r=b-Ap (p is initial guess)
- $\upsilon \rho = r^T r$ , check if already solved
- v s=r (first search direction)
- υ **Loop**:
  - t=As
  - $\alpha = \rho/(s^{T}t)$  (optimum step size)
  - x+=  $\alpha$ s, r-=  $\alpha$ t, check for convergence
  - $\rho_{new} = r^T r$
  - $\beta = \rho_{new} / \rho$
  - $s=r+\beta s$  (updated search direction)
  - $\rho = \rho_{new}$

cs533d-term1-2005 37