

## Shallow water equations

- ◆ From last time, using eta for depth= $h+H$ :

$$\frac{D\eta}{Dt} = -\eta \nabla \cdot u$$

$$\frac{Du}{Dt} = -g \nabla h$$

- ◆ We'll discretize this using "splitting"
  - Handle the material derivative first, then the right-hand side terms next
  - Intermediate depth and velocity from just the advection part

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## Advection

- ◆ Let's discretize just the material derivative (advection equation):

$$q_t + u \cdot \nabla q = 0 \quad \text{or} \quad \frac{Dq}{Dt} = 0$$

- ◆ For a Lagrangian scheme this is trivial: just move the particle that stores  $q$ , don't change the value of  $q$  at all

$$q(x(t), t) = q(x_0, 0)$$

- ◆ For Eulerian schemes it's not so simple

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## Scalar advection in 1D

- ◆ Let's simplify even more, to just one dimension:  $q_t + u q_x = 0$
- ◆ Further assume  $u = \text{constant}$
- ◆ And let's ignore boundary conditions for now
  - E.g. use a periodic boundary
- ◆ True solution just translates  $q$  around at speed  $u$  - shouldn't change shape

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## First try: central differences

- ◆ Centred-differences give better accuracy
  - More terms cancel in Taylor series
- ◆ Example: 
$$\frac{\partial q_i}{\partial t} = -u \left( \frac{q_{i+1} - q_{i-1}}{2\Delta x} \right)$$
  - 2nd order accurate in space
- ◆ Eigenvalues are pure imaginary - rules out Forward Euler and RK2 in time
- ◆ But what does the solution look like?

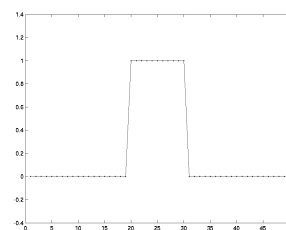
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## Testing a pulse

- ◆ We know things have to work out nicely in the limit (second order accurate)
  - I.e. when the grid is fine enough
  - What does that mean? -- when the sampled function looks smooth on the grid
- ◆ In graphics, it's just redundant to use a grid that fine
  - we can fill in smooth variations with interpolation later
- ◆ So we're always concerned about coarse grids == not very smooth data
- ◆ Discontinuous pulse is a nice test case

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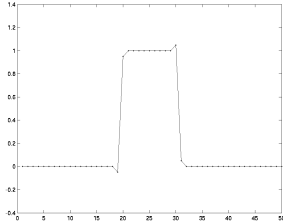
## A pulse (initial conditions)



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## Centered finite differences

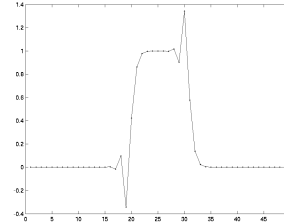
- ◆ A few time steps (RK4, small  $\Delta t$ ) later
  - $u=1$ , so pulse should just move right without changing shape



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## Centred finite differences

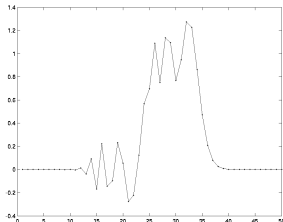
- ◆ A little bit later...



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## Centred finite differences

- ◆ A fair bit later



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## What went wrong?

- ◆ Lots of ways to interpret this error
- ◆ Example - phase analysis
  - Take a look at what happens to a sinusoid wave numerically
  - The amplitude stays constant (good), but the wave speed depends on wave number (bad) - we get dispersion
  - So the sinusoids that initially sum up to be a square pulse move at different speeds and separate out
    - We see the low frequency ones moving faster...
  - But this analysis won't help so much in multi-dimensions, variable  $u$ ...

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## Modified PDE's

- ◆ Another way to interpret error - try to account for it in the physics
- ◆ Look at truncation error more carefully:

$$q_{i+1} = q_i + \Delta x \frac{\partial q}{\partial x} + \frac{\Delta x^2}{2} \frac{\partial^2 q}{\partial x^2} + \frac{\Delta x^3}{6} \frac{\partial^3 q}{\partial x^3} + O(\Delta x^4)$$

$$q_{i-1} = q_i - \Delta x \frac{\partial q}{\partial x} + \frac{\Delta x^2}{2} \frac{\partial^2 q}{\partial x^2} - \frac{\Delta x^3}{6} \frac{\partial^3 q}{\partial x^3} + O(\Delta x^4)$$

$$\frac{q_{i+1} - q_{i-1}}{2\Delta x} = \frac{\partial q}{\partial x} + \frac{\Delta x^2}{6} \frac{\partial^3 q}{\partial x^3} + O(\Delta x^3)$$

- ◆ Up to high order error, we numerically solve

$$q_t + uq_x = -\frac{u\Delta x^2}{6} q_{xxx}$$

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## Interpretation

$$q_t + uq_x = -\frac{u\Delta x^6}{6} q_{xxx}$$

- ◆ Extra term is "dispersion"
  - Does exactly what phase analysis tells us
  - Behaves a bit like surface tension...
- ◆ We want a numerical method with a different sort of truncation error
  - Any centred scheme ends up giving an odd truncation error --- dispersion
- ◆ Let's look at one-sided schemes

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# Upwind differencing

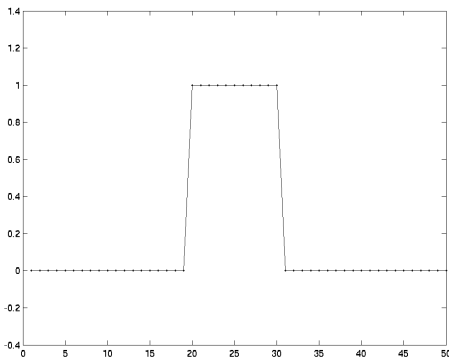
- ◆ Think physically:
  - True solution is that  $q$  just translates at velocity  $u$
- ◆ Information flows with  $u$
- ◆ So to determine future values of  $q$  at a grid point, need to look “upwind” -- where the information will blow from
  - Values of  $q$  “downwind” only have any relevance if we know  $q$  is smooth -- and we’re assuming it isn’t

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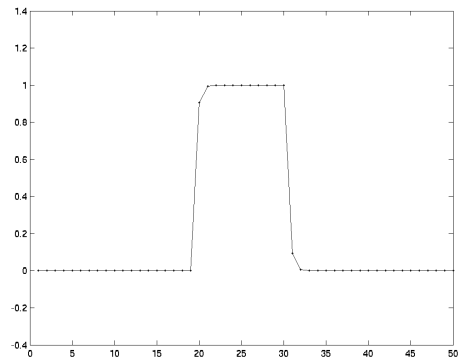
# 1st order upwind

- ◆ Basic idea: look at sign of  $u$  to figure out which direction we should get information
- ◆ If  $u < 0$  then  $\partial q / \partial x \approx (q_{i+1} - q_i) / \Delta x$
- ◆ If  $u > 0$  then  $\partial q / \partial x \approx (q_i - q_{i-1}) / \Delta x$
- ◆ Only 1st order accurate though
  - Let’s see how it does on the pulse...

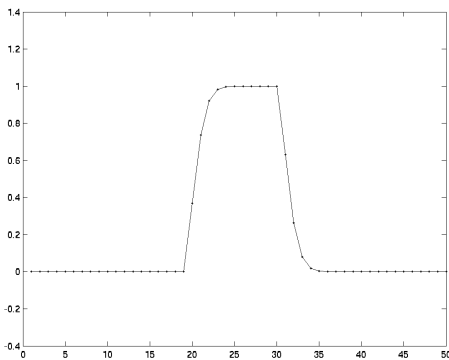
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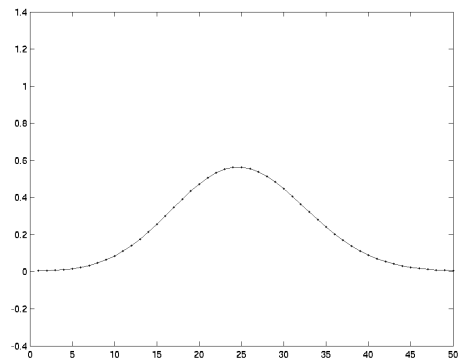
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## Modified PDE again

- ◆ Let's see what the modified PDE is this time

$$q_{i+1} = q_i + \Delta x \frac{\partial q}{\partial x} + \frac{\Delta x^2}{2} \frac{\partial^2 q}{\partial x^2} + O(\Delta x^3)$$

$$\frac{q_{i+1} - q_i}{\Delta x} = \frac{\partial q}{\partial x} + \frac{\Delta x}{2} \frac{\partial^2 q}{\partial x^2} + O(\Delta x^2)$$

- ◆ For  $u < 0$  then we have  $q_i + uq_x = -\frac{u\Delta x}{2} q_{xx}$
- ◆ And for  $u > 0$  we have (basically flip sign of  $\Delta x$ )  

$$q_i + uq_x = \frac{u\Delta x}{2} q_{xx}$$
- ◆ Putting them together, 1st order upwind numerical solves (to 2nd order accuracy)

$$q_i + uq_x = \left| \frac{u\Delta x}{2} \right| q_{xx}$$

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## Interpretation

- ◆ The extra term (that disappears as we refine the grid) is **diffusion** or **viscosity**
- ◆ So sharp pulse gets blurred out into a hump, and eventually melts to nothing
- ◆ It looks a lot better, but still not great
  - Again, we want to pack as much detail as possible onto our coarse grid
  - With this scheme, the detail melts away to nothing pretty fast
- ◆ Note: unless grid is really fine, the numerical viscosity is much larger than physical viscosity - so might as well not use the latter

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## Fixing upwind method

- ◆ Natural answer - reduce the error by going to higher order - but life isn't so simple
- ◆ High order difference formulas can overshoot in extrapolating
  - If we difference over a discontinuity
  - Stability becomes a real problem
- ◆ Go nonlinear (even though problem is linear)
  - "limiters" - use high order unless you detect a (near-)overshoot, then go back to 1st order upwind
  - "ENO" - try a few different high order formulas, pick smoothest

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## Hamilton-Jacobi Equations

- ◆ In fact, the advection step is a simple example of a Hamilton-Jacobi equation (HJ)
  - $q_t + H(q, q_x) = 0$
- ◆ Come up in lots of places
  - Level sets...
- ◆ Lots of research on them, and numerical methods to solve them
  - E.g. 5th order HJ-WENO
- ◆ We don't want to get into that complication

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## Other problems

- ◆ Even if we use top-notch numerical methods for HJ, we have problems
  - Time step limit: CFL condition
    - Have to pick time step small enough that information physically moves less than a grid cell:  
 $\Delta t < \Delta x / u$
  - Schemes can get messy at boundaries
  - Discontinuous data still gets smoothed out to some extent (high resolution schemes drop to first order upwinding)

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## Exploiting Lagrangian view

- ◆ But wait! This was trivial for Lagrangian (particle) methods!
- ◆ We still want to stick an Eulerian grid for now, but somehow exploit the fact that
  - If we know  $q$  at some point  $x$  at time  $t$ , we just follow a particle through the flow starting at  $x$  to see where that value of  $q$  ends up

$$q(x(t + \Delta t), t + \Delta t) = q(x(t), t)$$

$$\frac{dx}{dt} = u(x), \quad x(t) = x_0$$

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## Looking backwards

- ◆ Problem with tracing particles - we want values at **grid nodes** at the end of the step
  - Particles could end up anywhere
- ◆ But... we can look backwards in time

$$q_{ijk} = q(x(t - \Delta t), t - \Delta t)$$

$$\frac{dx}{dt} = u(x), \quad x(t) = x_{ijk}$$

- ◆ Same formulas as before - but new interpretation
  - To get value of q at a grid point, follow a particle backwards through flow to wherever it started

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## Semi-Lagrangian method

- ◆ Developed in weather prediction, going back to the 50's
- ◆ Also dubbed "stable fluids" in graphics (reinvention by Stam '99)
- ◆ To find new value of q at a grid point, trace particle backwards from grid point (with velocity u) for  $-\Delta t$  and interpolate from old values of q
- ◆ Two questions
  - How do we trace?
  - How do we interpolate?

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## Tracing

- ◆ The errors we make in tracing backwards aren't too big a deal
  - We don't compound them - stability isn't an issue
  - How accurate we are in tracing doesn't effect shape of q much, just location
    - Whether we get too much blurring, oscillations, or a nice result is really up to interpolation
- ◆ Thus look at "Forward" Euler and RK2

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## Tracing: 1st order

- ◆ We're at grid node (i,j,k) at position  $x_{ijk}$
- ◆ Trace backwards through flow for  $-\Delta t$ 

$$x_{old} = x_{ijk} - \Delta t u_{ijk}$$
  - Note - using u value at grid point (what we know already) like Forward Euler.
- ◆ Then can get new q value (with interpolation)

$$q_{ijk}^{n+1} = q^n(x_{old})$$

$$= q^n(x_{ijk} - \Delta t u_{ijk})$$

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## Interpolation

- ◆ "First" order accurate: nearest neighbour
  - Just pick q value at grid node closest to  $x_{old}$
  - Doesn't work for slow fluid (small time steps) -- nothing changes!
  - When we divide by grid spacing to put in terms of advection equation, drops to zero'th order accuracy
- ◆ "Second" order accurate: linear or bilinear (2D)
  - Ends up first order in advection equation
  - Still fast, easy to handle boundary conditions...
  - How well does it work?

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## Linear interpolation

- ◆ Error in linear interpolation is proportional to

$$\Delta x^2 \frac{\partial^2 q}{\partial x^2}$$

- ◆ Modified PDE ends up something like...

$$\frac{Dq}{Dt} = k(\Delta t) \Delta x^2 \frac{\partial^2 q}{\partial x^2}$$

- We have numerical viscosity, things will smear out
- For reasonable time steps, k looks like  $1/\Delta t \sim 1/\Delta x$
- ◆ [Equivalent to 1st order upwind for CFL  $\Delta t$ ]
- ◆ In practice, too much smearing for inviscid fluids

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## Nice properties of lerping

- ◆ Linear interpolation is completely stable
  - Interpolated value of  $q$  must lie between the old values of  $q$  on the grid
  - Thus with each time step,  $\max(q)$  cannot increase, and  $\min(q)$  cannot decrease
- ◆ Thus we end up with a fully stable algorithm - take  $\Delta t$  as big as you want
  - Great for interactive applications
  - Also simplifies whole issue of picking time steps

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## Cubic interpolation

- ◆ To fix the problem of excessive smearing, go to higher order
- ◆ E.g. use cubic splines
  - Finding interpolating  $C^2$  cubic spline is a little painful, an alternative is the
  - $C^1$  Catmull-Rom (cubic Hermite) spline
    - [derive]
- ◆ Introduces overshoot problems
  - Stability isn't so easy to guarantee anymore

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## Min-mod limited Catmull-Rom

- ◆ See Fedkiw, Stam, Jensen '01
- ◆ Trick is to check if either slope at the endpoints of the interval has the wrong sign
  - If so, clamp the slope to zero
  - Still use cubic Hermite formulas with more reliable slopes
- ◆ This has same stability guarantee as linear interpolation
  - But in smoother parts of flow, higher order accurate
  - Called "high resolution"
- ◆ Still has issues with boundary conditions...

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## Back to Shallow Water

- ◆ So we can now handle advection of both water depth and each component of water velocity
- ◆ Left with the divergence and gradient terms

$$\frac{\partial \eta}{\partial t} = -\eta \left( \frac{\partial u}{\partial x} + \frac{\partial w}{\partial z} \right)$$

$$\frac{\partial u}{\partial t} = -g \frac{\partial h}{\partial x}$$

$$\frac{\partial w}{\partial t} = -g \frac{\partial h}{\partial z}$$

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## MAC grid

- ◆ We like central differences - more accurate, unbiased
- ◆ So natural to use a staggered grid for velocity and height variables
  - Called MAC grid after the Marker-and-Cell method (Harlow and Welch '65) that introduced it
- ◆ Heights at cell centres
- ◆ u-velocities at x-faces of cells
- ◆ w-velocities at z-faces of cells

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## Spatial Discretization

- ◆ So on the MAC grid:

$$\frac{\partial \eta_{ij}}{\partial t} = -\eta_{ij} \left( \frac{u_{i+\frac{1}{2},j} - u_{i-\frac{1}{2},j}}{\Delta x} + \frac{w_{i,j+\frac{1}{2}} - w_{i,j-\frac{1}{2}}}{\Delta z} \right)$$

$$\frac{\partial u_{i+\frac{1}{2},j}}{\partial t} = -g \frac{h_{i+1,j} - h_{i,j}}{\Delta x}$$

$$\frac{\partial w_{i,j+\frac{1}{2}}}{\partial t} = -g \frac{h_{i,j+1} - h_{i,j}}{\Delta z}$$

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