

Notes

Shells

- ◆ Simple addition to previous bending formulation: allow for nonzero rest angles
 - i.e. rest state is curved
 - Called a “shell” model
- ◆ Instead of curvature squared, take curvature difference squared
 - Instead of θ , use $\theta - \theta_0$

Rayleigh damping

- ◆ Start with variational formulation:
W is discrete elastic potential energy
- ◆ Suppose W is of the form $W = \frac{1}{2} k C^T A C$
 - C is a vector that is zero at undeformed state
 - A is a matrix measuring the length/area/volume of integration for each element of C

- ◆ Then elastic force is $F_{elastic} = -k \frac{\partial C^T}{\partial x} A C$

- C says how much force, $\partial C / \partial X$ gives the direction

- ◆ Damping should be in the same direction, and proportional to $\partial C / \partial t$:

$$F_{damping} = -d \frac{\partial C^T}{\partial x} A \frac{\partial C}{\partial t}$$

- ◆ Chain rule:

- Linear in v, but not in x... $= -d \frac{\partial C^T}{\partial x} A \frac{\partial C}{\partial x} v$

Cloth modeling

- ◆ Putting what we have so far together: cloth
- ◆ Appropriately scaled springs + bending
- ◆ Issues left to cover:
 - Time steps and stability
 - Extra spring tricks
 - Collisions

Spring timesteps

◆ For a fully explicit method:

- Elastic time step limit is

$$\Delta t \sim O\left(\sqrt{\frac{mL^2}{EA}}\right) = O\left(\frac{1}{n}\right)$$

- Damping time step limit is

$$\Delta t \sim O\left(\frac{mL^2}{DA}\right) = O\left(\frac{1}{n^2}\right)$$

- What does this say about scalability?

Bending timesteps

◆ Back of the envelope from discrete energy:

$$\frac{\partial a}{\partial x} \sim \frac{1}{m} B \frac{|e|^2}{A} \frac{\partial^2 \theta}{\partial x^2} = O\left(\frac{L^2}{L^2 L^2}\right)$$

$$\Delta t = O\left(\frac{1}{n^2}\right)$$

◆ Or from 1D bending problem

- [practice variational derivatives]

Fourth order problems

◆ Linearize and simplify drastically, look for steady-state solution (F=0): spline equations

- Essentially 4th derivatives are zero
- Solutions are (bi-)cubics

◆ Model (nonsteady) problem: $x_{tt} = -x_{pppp}$

- Assume solution $x(p, t) = e^{\sqrt{-1}k(p-ct)}$

Wave of spatial frequency k , moving at speed c

- [solve for wave parameters]
- Dispersion relation: small waves move really fast
- CFL limit (and stability): for fine grids, BAD
- Thankfully, we rarely get that fine

Implicit/Explicit Methods

◆ Implicit bending is painful

◆ In graphics, usually unnecessary

- Dominant forces on the grid resolution we use tend to be the 2nd order terms: stretching etc.

◆ But nice to go implicit to avoid time step restriction for stretching terms

◆ No problem: treat some terms (bending) explicitly, others (stretching) implicitly

- $v_{n+1} = v_n + \Delta t/m(F_1(x_n, v_n) + F_2(x_{n+1}, v_{n+1}))$
- All bending is in F_1 , half the elastic stretch in F_1 , half the elastic stretch in F_2 , all the damping in F_2

Hacking in strain limits

- ◆ Especially useful for cloth:
 - Biphasic nature: won't easily extend past a certain point
- ◆ Sweep through elements (e.g. springs)
 - If strain is beyond given limit, apply force to return it to closest limit
 - Also damp out strain rate to zero
- ◆ No stability limit for fairly stiff behaviour
 - But mesh-independence is an issue...
- ◆ See X. Provat, "Deformation constraints in a mass-spring model to describe rigid cloth behavior", Graphics Interface '95

Extra effects with springs

- ◆ (Brittle) fracture
 - When a spring is stretched too far, break it
 - Issue with loose ends...
- ◆ Plasticity
 - Whenever a spring is stretched too far, change the rest length part of the way
- ◆ More on this later